

The *Ivory* Optomechanical Modeling Tools

Alson E. Hatheway Inc.

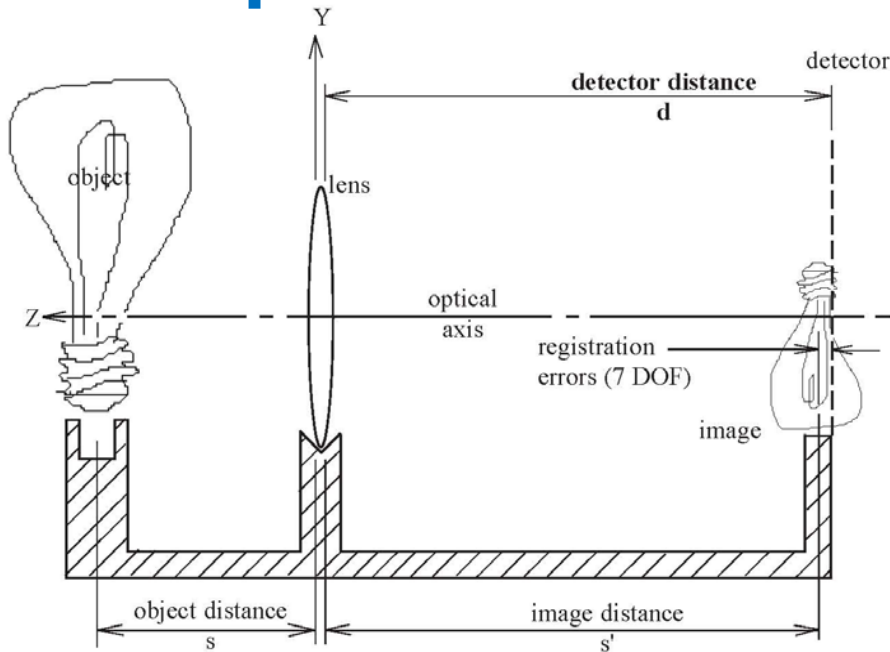
e: teale@eahinc.com



AEH.

Optomechanics

An Optomechanical System



Ivory determines changes in the position, orientation and size of the image on the detector.

There are seven image registration variables on the detector:

2 decenters, T_{x_i} and T_{y_i}

1 defocus, T_{z_i}

2 tips, R_{x_i} and R_{y_i}

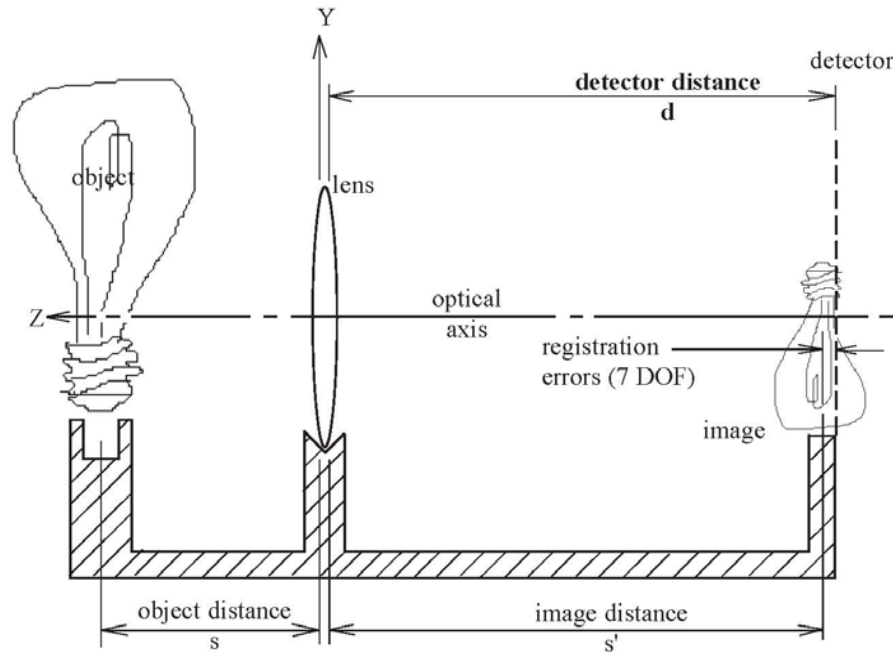
1 rotation, R_{z_i}

1 change in size, $\Delta M/M_i$

AEH.

Optomechanics

The Optomechanical Constraint Equations



The Optomechanical Constraint Equations

determine the magnitude of these seven registration variables:

$$Tx_i = Tx_1(\partial Tx_i / \partial Tx_1) + Ty_1(\partial Tx_i / \partial Ty_1) + Tz_1(\partial Tx_i / \partial Tz_1) + Rx_1(\partial Tx_i / \partial Rx_1) + \dots$$

$$Ty_i = Tx_1(\partial Ty_i / \partial Tx_1) + Ty_1(\partial Ty_i / \partial Ty_1) + Tz_1(\partial Ty_i / \partial Tz_1) + Rx_1(\partial Ty_i / \partial Rx_1) + \dots$$

$$Tz_i = Tx_1(\partial Tz_i / \partial Tx_1) + Ty_1(\partial Tz_i / \partial Ty_1) + Tz_1(\partial Tz_i / \partial Tz_1) + Rx_1(\partial Tz_i / \partial Rx_1) + \dots$$

$$Rx_i = Tx_1(\partial Rx_i / \partial Tx_1) + Ty_1(\partial Rx_i / \partial Ty_1) + Tz_1(\partial Rx_i / \partial Tz_1) + Rx_1(\partial Rx_i / \partial Rx_1) + \dots$$

$$Ry_i = Tx_1(\partial Ry_i / \partial Tx_1) + Ty_1(\partial Ry_i / \partial Ty_1) + Tz_1(\partial Ry_i / \partial Tz_1) + TRx_1(\partial Ry_i / \partial Rx_1) + \dots$$

$$Rz_i = Tx_1(\partial Rz_i / \partial Tx_1) + Ty_1(\partial Rz_i / \partial Ty_1) + Tz_1(\partial Rz_i / \partial Tz_1) + Rx_1(\partial Rz_i / \partial Rx_1) + \dots$$

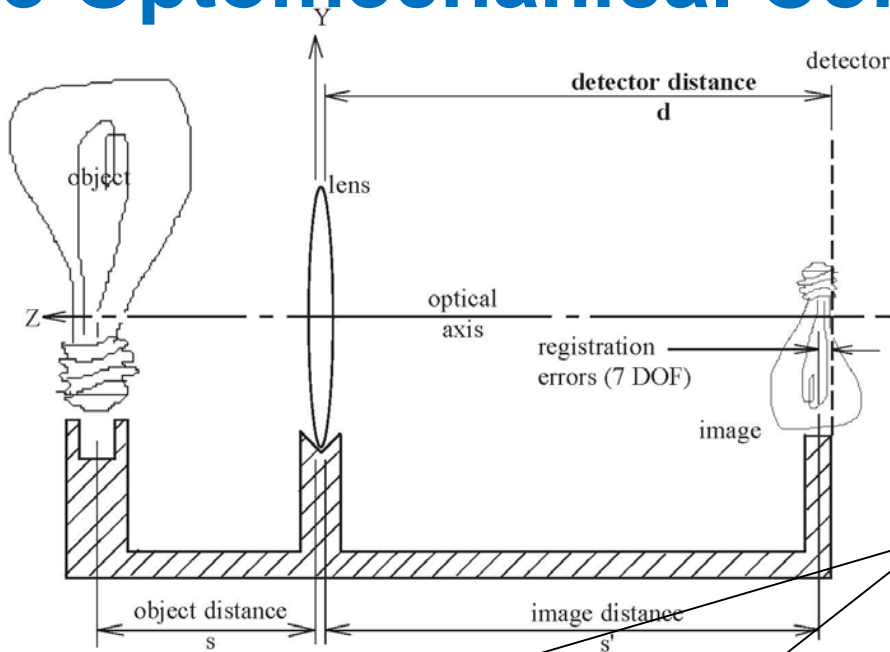
$$\Delta M_i / M_i = Tx_1(\partial M / M / \partial Tx_1) + Ty_1(\partial M / M / \partial Ty_1) + Tz_1(\partial M / M / \partial Tz_1) + \dots$$

AEH.

The partial derivatives are called “influence coefficients” (ICs).

Optomechanics

The Optomechanical Constraint Equations



The ICs for a single lens are calculated from its magnification, M , its focal length, f , and distance between its principal points, p (the principal thickness).

The ICs are assigned to the first principal point of each optical element.

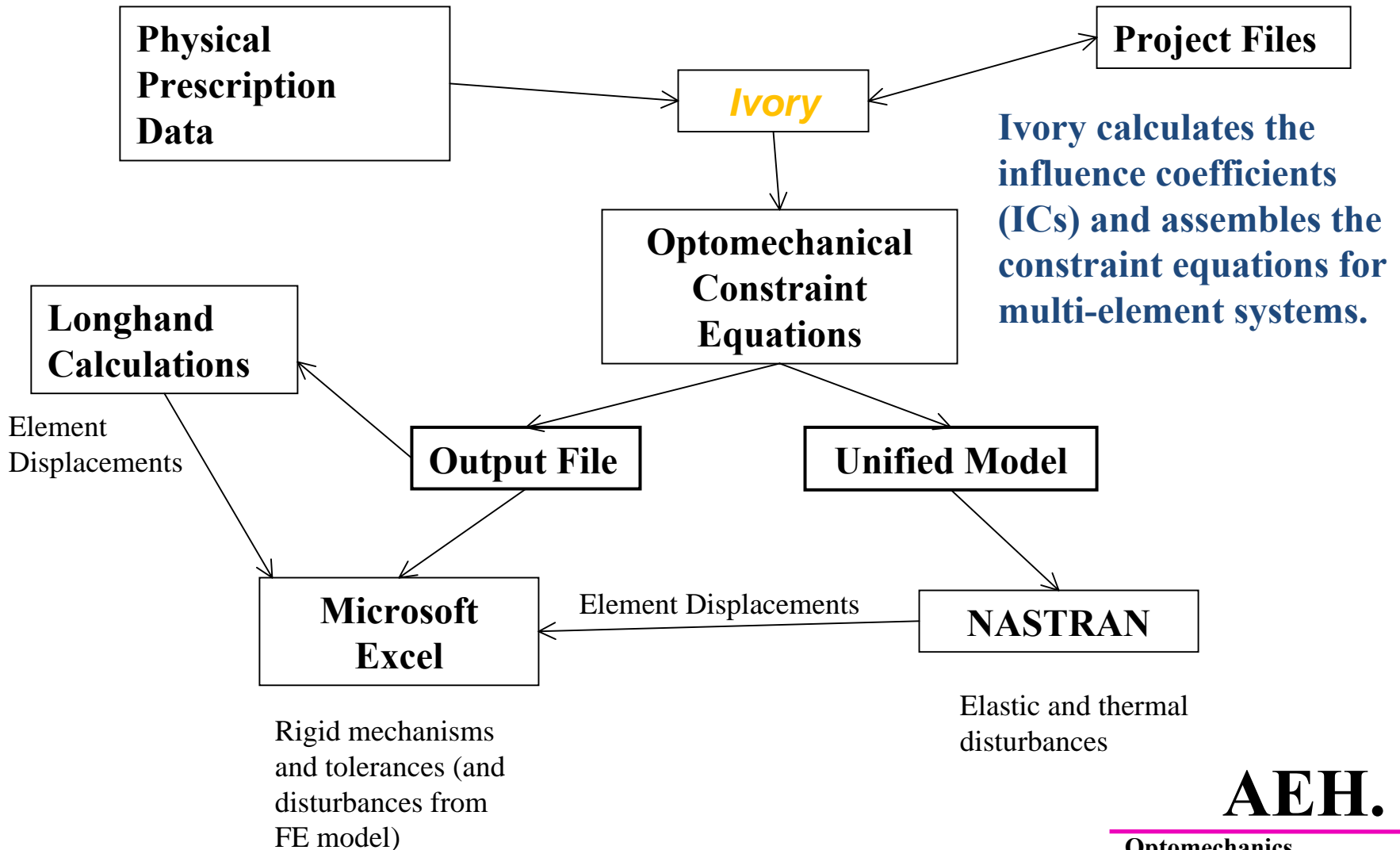
$$\begin{matrix}
 \begin{matrix} M \\ \\ \\ \\ \\ \\ M/f \end{matrix} \\
 \begin{matrix} Tx \\ Ty \\ Tz \\ Rx \\ Ry \\ Rz \end{matrix} \\
 \text{Object Displacements}
 \end{matrix}
 +
 \begin{matrix}
 \begin{matrix} 1-M & -p \\ \\ 1-M & p \\ \\ 1-M^2 & & -(M-1)^2 \\ \\ 1-M & & & \\ \\ 1-M & & & & \\ \\ 0.0 \\ \\ -M/f & & & & (1-M)/f \end{matrix} \\
 \begin{matrix} Tx \\ Ty \\ Rz \\ Rx \\ Ry \\ Rz \\ \Delta f \end{matrix} \\
 \text{Lens Displacements}
 \end{matrix}
 +
 \begin{matrix}
 \begin{matrix} -1 \\ \\ -1 \\ \\ -1 \\ \\ -1 \end{matrix} \\
 \begin{matrix} Tx \\ Ty \\ Tz \\ Rx \\ Ry \\ Rz \end{matrix} \\
 \text{Detector Displacements}
 \end{matrix}
 =
 \begin{matrix}
 \begin{matrix} Tx \\ Ty \\ Tz \\ Rx \\ Ry \\ Rz \\ \Delta M/M \end{matrix} \\
 \text{Registration Variables}
 \end{matrix}$$

Registration Variables

AEH.

Optomechanics

Ivory Optomechanical Modeling Tools



AEH.

Optomechanics

Example, an IR Imager



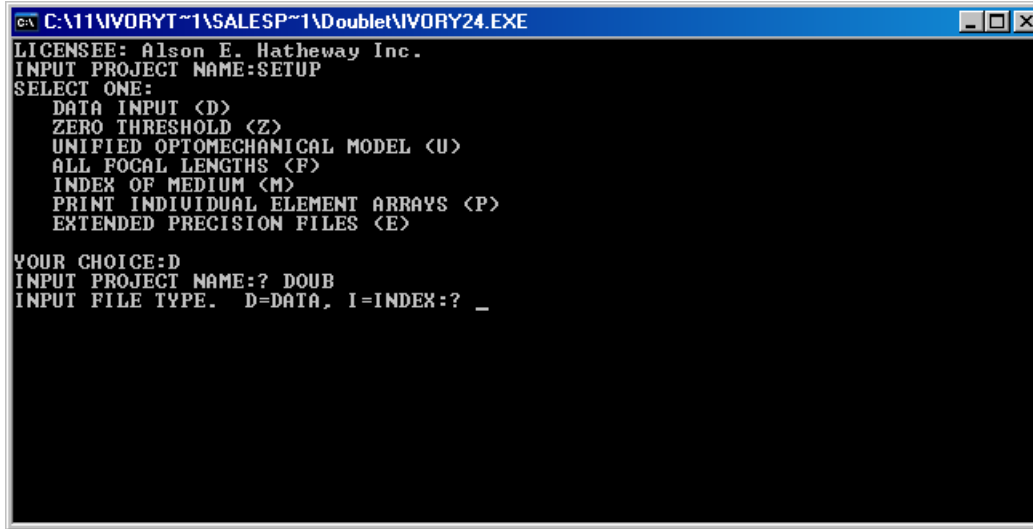
Surf	Elem	Radius	Index	Thickness
1	obj	inf	AIR	-inf
2	1	3.5	ge	-.25
3	1	5.	AIR	-2.67
4	2	1.5	ge	-.2
5	2	1	AIR	-.674
6	det	inf	AIR	0.0

AEH.

Optomechanics

The *Ivory* Input Files

Open *Ivory*. Enter SETUP. It helps to prepare the prescription data in two “project” files.



```
C:\11\IVORYT~1\SALESP~1\Doublet\IVORY24.EXE
LICENSEE: Alson E. Hatheway Inc.
INPUT PROJECT NAME: SETUP
SELECT ONE:
  DATA INPUT <D>
  ZERO THRESHOLD <Z>
  UNIFIED OPTOMECHANICAL MODEL <U>
  ALL FOCAL LENGTHS <F>
  INDEX OF MEDIUM <M>
  PRINT INDIVIDUAL ELEMENT ARRAYS <P>
  EXTENDED PRECISION FILES <E>

YOUR CHOICE: D
INPUT PROJECT NAME: ? DOUB
INPUT FILE TYPE. D=DATA, I=INDEX: ? _
```

Ivory operates from the command prompt window.

It helps format the “project” files from the optical prescription.

The first, “doub.dat,” contains the geometry data.

Surf	Elem	Radius	Index	Thickness	Type	f1	f2	f3	f4
1	obj	inf	AIR	inf	obj	1.0000000	0.0000000	0.0000000	0.0000000
2	1	-3.5	ge	.25	LENS	0.0000000	0.0000000	0.0000000	0.0000000
3	1	-5.	AIR	2.67	LENS	0.0000000	0.0000000	0.0000000	0.0000000
4	2	-1.5	ge	.2	LENS	0.0000000	0.0000000	0.0000000	0.0000000
5	2	-1	AIR	.674	LENS	0.0000000	0.0000000	0.0000000	0.0000000
6	det	inf	AIR	0.0	det				

The second, “doub.ind,” contains the index of refraction data.

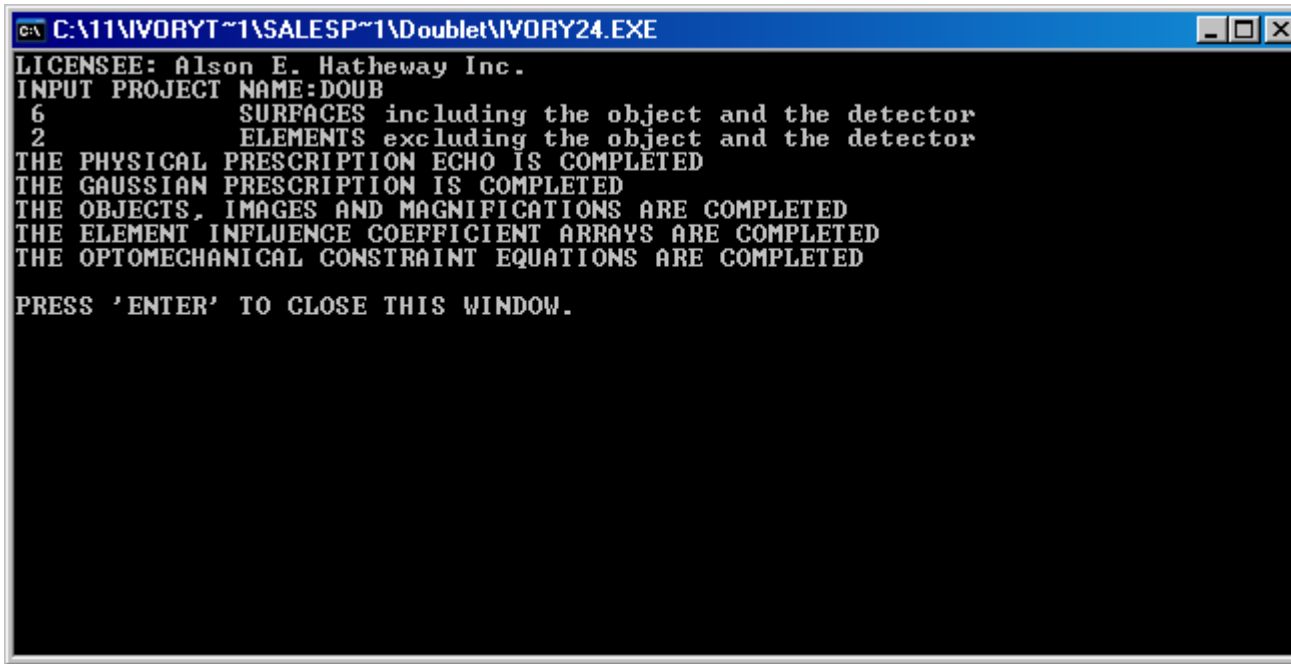
MATERIAL	INDEX
AIR	1.0
ge	4.00024

AEH.

Optomechanics

Running *Ivory*

Open *Ivory*. At the prompt for a “project” name enter “doub.”



```
C:\11\IVORYT~1\SALESP~1\Doublet\IVORY24.EXE
LICENSEE: Alson E. Hatheway Inc.
INPUT PROJECT NAME:DOUB
 6          SURFACES including the object and the detector
 2          ELEMENTS excluding the object and the detector
THE PHYSICAL PRESCRIPTION ECHO IS COMPLETED
THE GAUSSIAN PRESCRIPTION IS COMPLETED
THE OBJECTS, IMAGES AND MAGNIFICATIONS ARE COMPLETED
THE ELEMENT INFLUENCE COEFFICIENT ARRAYS ARE COMPLETED
THE OPTOMECHANICAL CONSTRAINT EQUATIONS ARE COMPLETED
PRESS 'ENTER' TO CLOSE THIS WINDOW.
```

Ivory runs the project files to produce the Optomechanical Constraint Equations in its output file.

Ivory has calculated the optomechanical constraint equations and written them to the “doub.out” file.

AEH.

Optomechanics

The Top of Ivory's "doub.out" File

Output from -

IVORY Optomechanical Modeling Tools

Version 2.4

Copyright 2010, Alson E. Hatheway Inc.

This Product has been licensed to Alson E. Hatheway Inc. for one user(s).

PROJECT NAME: 'doub' TIME AND DATE: 17:42:35 02-19-2010

PHYSICAL PRESCRIPTION ECHO

Surf	Elem	Radius	Index	Thickness	Type	f1	f2	f3	f4
1	obj	inf	1.0	inf	obj	1	0	0	0
2	1	-3.5	4.00024	.25	LENS	0	0	0	0
3	1	-5	1.0	2.67	LENS	0	0	0	0
4	2	-1.5	4.00024	.2	LENS	0	0	0	0
5	2	-1	1.0	.674	LENS	0	0	0	0
6	det	inf	1.0	0	det				

INDEXES OF REFRACTION ARE RELATIVE TO THE VALUE OF 1.000292

GAUSSIAN PRESCRIPTION

ELE	F	H1	H2	P	P/AIR	PHI	THETA	TYPE
obj	0	0	0	0	inf	0	0	obj
1	3.456506	.1296216	.1851736	.1944479	3.069449	0	0	LENS
2	-1.42847	-.2142747	-.1428498	.1285751	.5311502	0	0	LENS
det	0	0	0	0	0	0	0	det

SYSTEM 4.7411690902 10.317288630 4.0674066621 9.3698825682 4.7414066621

effective focal length

Ivory's optical quality checks in the output file

OBJECTS, IMAGES AND MAGNIFICATIONS

ELE	F	S	S'	M	PHI	THETA	TYPE	e/Tzo
obj	inf	0	0	+1.0000	0	0	obj	
1	3.456506	inf	-3.4565	0	0	0	LENS	+0.00D+00
2	-1.42847	-0.3871	-0.5309	+1.3717	0	0	LENS	-9.60D-01
det	inf	+2.38D-04	+2.38D-04	+1.0	0	0	det	

residual focus error

AEH.

Optomechanics

The Bottom of *Ivory's* "doub.out" File

OPTOMECHANICAL CONSTRAINT EQUATIONS

(ABSOLUTE VALUES SMALLER THAN 0 ARE PRINTED AS 0.0)

	REGISTRATION VARIABLES								
	TX	TY	TZ	RX	RY	RZ	DM/M	Df ,p	LDesVar
Tx	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Dt
Ty	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	DR1
Tz	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	DR2
Rx	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Dn
Ry	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Rz	0.0	0.0	0.0	0.0	0.0	+1.00000	0.0	0.0	
Df ,p	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
SYSTEM-OBJECT									
Tx	+1.37167	0.0	0.0	0.0	0.0	0.0	0.0	-1.53625	Dt
Ty	0.0	+1.37167	0.0	0.0	0.0	0.0	0.0	-3.03587	DR1
Tz	0.0	0.0	+1.88146	0.0	0.0	0.0	-0.96023	+1.35699	DR2
Rx	0.0	+0.26672	0.0	+1.37167	0.0	0.0	0.0	-1.18408	Dn
Ry	-0.26672	0.0	0.0	0.0	+1.37167	0.0	0.0	0.0	
Rz	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Df ,p	0.0	0.0	-1.88146	0.0	0.0	0.0	+1.24954	0.0	
ELEMENT-1									
Tx	-0.37167	0.0	0.0	0.0	0.0	0.0	0.0	-3.06110	Dt
Ty	0.0	-0.37167	0.0	0.0	0.0	0.0	0.0	-3.12907	DR1
Tz	0.0	0.0	-0.88146	0.0	0.0	0.0	+0.96023	+5.50985	DR2
Rx	0.0	+0.12858	0.0	-0.37167	0.0	0.0	0.0	+0.42511	Dn
Ry	-0.12858	0.0	0.0	0.0	-0.37167	0.0	0.0	0.0	
Rz	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Df ,p	0.0	0.0	-0.13813	0.0	0.0	0.0	+0.26018	0.0	
ELEMENT-2									
Tx	-1.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Dt
Ty	0.0	-1.00000	0.0	0.0	0.0	0.0	0.0	0.0	DR1
Tz	0.0	0.0	-1.00000	0.0	0.0	0.0	0.0	0.0	DR2
Rx	0.0	0.0	0.0	-1.00000	0.0	0.0	0.0	0.0	Dn
Ry	0.0	0.0	0.0	0.0	-1.00000	0.0	0.0	0.0	
Rz	0.0	0.0	0.0	0.0	0.0	-1.00000	0.0	0.0	
Df ,p	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
DETECTOR									

The Optomechanical Constraint Equations for the seven registration variables.

Thank you for using IVORY(tm) to prepare the Optomechanical Constraint Equations for 'doub'.

AEH.

Optomechanics

Position Tolerances in Excel...

OPTOMECH CONSTRAIN EQUATION (ABSOLUTE VALUES SMALLER THAN 0 ARE PRINTED AS 0.0)

REGISTRAR VARIABLES										IMAGE MOTION CONTRIBUTIONS							
	TX	TY	TZ	RX	RY	RZ	DM/M	Df,p	LDesVar								
	Tx	0	0	0	0	0	0	0	0	0	Dt	0	0	0	0	0	0
	Ty	0	0	0	0	0	0	0	0	0	DR1	0	0	0	0	0	0
	Tz	0	0	0	0	0	0	0	0	0	DR2	0	0	0	0	0	0
	Rx	0	0	0	0	0	0	0	0	0	Dn	0	0	0	0	0	0
	Ry	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	Rz	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0
	Df,p	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	SYSTEM-OBJECT																
	Tx	1.3717	0	0	0	0	0	0	-1.5363	Dt	3.00E-03	0.004115	0	0	0	0	0
	Ty	0	1.3717	0	0	0	0	0	-3.0359	DR1	3.00E-03	0	0.004115	0	0	0	0
	Tz	0	0	1.8815	0	0	0	-0.9602	1.357	DR2	3.00E-03	0	0	0.005645	0	0	0.002881
	Rx	0	0.2667	0	1.3717	0	0	0	-1.1841	Dn	1.75E-03	0	0.000467	0	0.002400475	0	0
	Ry	-0.2667	0	0	0	1.3717	0	0	0	0	1.75E-03	0.000467	0	0	0	0.002400475	0
	Rz	0	0	0	0	0	0	0	0	0	1.75E-03	0	0	0	0	0	0
	Df,p	0	0	-1.8815	0	0	0	1.2495	0	0	0	0	0	0	0	0	0
	ELEMENT-1																
	Tx	-0.3717	0	0	0	0	0	0	-3.0611	Dt	3.00E-03	0.001115	0	0	0	0	0
	Ty	0	-0.3717	0	0	0	0	0	-3.1291	DR1	3.00E-03	0	0.001115	0	0	0	0
	Tz	0	0	-0.8815	0	0	0	0.9602	5.5099	DR2	3.00E-03	0	0	0.002645	0	0	0.002881
	Rx	0	0.1286	0	-0.3717	0	0	0	0.4251	Dn	1.75E-03	0	0.000225	0	0.000650475	0	0
	Ry	-0.1286	0	0	0	-0.3717	0	0	0	0	1.75E-03	0.000225	0	0	0	0.000650475	0
	Rz	0	0	0	0	0	0	0	0	0	1.75E-03	0	0	0	0	0	0
	Df,p	0	0	-0.1381	0	0	0	0.2602	0	0	0	0	0	0	0	0	0
	ELEMENT-2																
	Tx	-1	0	0	0	0	0	0	0	Dt	3.00E-03	0.003	0	0	0	0	0
	Ty	0	-1	0	0	0	0	0	0	DR1	3.00E-03	0	0.003	0	0	0	0
	Tz	0	0	-1	0	0	0	0	0	DR2	3.00E-03	0	0	0.003	0	0	0
	Rx	0	0	0	-1	0	0	0	0	Dn	1.75E-03	0	0	0	0.00175	0	0
	Ry	0	0	0	0	-1	0	0	0	0	1.75E-03	0	0	0	0	0.00175	0
	Rz	0	0	0	0	0	-1	0	0	0	1.75E-03	0	0	0	0	0	0.00175
	Df,p	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	DETECTOR																

TX	TY	TZ	RX	RY	RZ	DM/M
0.008922	0.008922	0.011289	0.00480095	0.00480095	0.00175	0.005761
ABSOLUTE WORST CASE IMAGE REGISTRATION ERRORS DUE TO ASSEMBLY						

Ivory's ICs
x position tolerances
elements' individual contributions

Worst case image registration
errors due to positioning
tolerances.

AEH.
Optomechanics

... + Lens Tolerances in Excel

OPTOMECH CONSTRAIN EQUATION (ABSOLUTE VALUES SMALLER THAN 0 ARE PRINTED AS 0.0)

REGISTRAT VARIABLES	TX	TY	TZ	RX	RY	RZ	DM/M	Df,p	LDesVar	Assumed Position Tol:	Assumed Lens Tol:	IMAGE MOTION CONTRIBUTIONS								
Tx	0	0	0	0	0	0	0	0	0 Dt			0	0	0	0	0	0	0	0	0
Ty	0	0	0	0	0	0	0	0	0 DR1			0	0	0	0	0	0	0	0	0
Tz	0	0	0	0	0	0	0	0	0 DR2			0	0	0	0	0	0	0	0	0
Rx	0	0	0	0	0	0	0	0	0 Dn			0	0	0	0	0	0	0	0	0
Ry	0	0	0	0	0	0	0	0	0			0	0	0	0	0	0	0	0	0
Rz	0	0	0	0	0	0	1	0	0			0	0	0	0	0	0	0	0	0
Df,p	0	0	0	0	0	0	0	0	0			0	0	0	0	0	0	0	0	0
SYSTEM-OBJECT												0	0	0	0	0	0	0	0	0
Tx	1.3717	0	0	0	0	0	0	0	-1.5363 Dt	3.00E-03	0.0025	0.004115	0	0	0	0	0	0	0	0
Ty	0	1.3717	0	0	0	0	0	0	-3.0359 DR1	3.00E-03	0.035	0	0.004115	0	0	0	0	0	0	0
Tz	0	0	1.8815	0	0	0	0	-0.9602	1.357 DR2	3.00E-03	0.05	0	0	0.005645	0	0	0	0	0.002881	0
Rx	0	0.2667	0	1.3717	0	0	0	0	-1.1841 Dn	1.75E-03	0.0001	0	0.000467	0	0.002400475	0	0	0	0	0
Ry	-0.2667	0	0	0	1.3717	0	0	0	0	1.75E-03		0.000467	0	0	0	0.002400475	0	0	0	0
Rz	0	0	0	0	0	0	0	0	0	1.75E-03		0	0	0	0	0	0	0	0	0
Df,p	0	0	-1.8815	0	0	0	0	1.2495	0	0.042366		0	0	0.079711	0	0	0	0	0	0.052936
ELEMENT-1												0	0	0	0	0	0	0	0	0
Tx	-0.3717	0	0	0	0	0	0	0	-3.0611 Dt	3.00E-03	0.002	0.001115	0	0	0	0	0	0	0	0
Ty	0	-0.3717	0	0	0	0	0	0	-3.1291 DR1	3.00E-03	0.015	0	0.001115	0	0	0	0	0	0	0
Tz	0	0	-0.8815	0	0	0	0	0.9602	5.5099 DR2	3.00E-03	0.01	0	0	0.002645	0	0	0	0	0.002881	0
Rx	0	0.1286	0	-0.3717	0	0	0	0	0.4251 Dn	1.75E-03	0.0001	0	0.000225	0	0.000650475	0	0	0	0	0
Ry	-0.1286	0	0	0	-0.3717	0	0	0	0	1.75E-03		0.000225	0	0	0	0.000650475	0	0	0	0
Rz	0	0	0	0	0	0	0	0	0	1.75E-03		0	0	0	0	0	0	0	0	0
Df,p	0	0	-0.1381	0	0	0	0	0.2602	0	0.002083		0	0	0.000288	0	0	0	0	0	0.000542
ELEMENT-2												0	0	0	0	0	0	0	0	0
Tx	-1	0	0	0	0	0	0	0	0 Dt	3.00E-03		0.003	0	0	0	0	0	0	0	0
Ty	0	-1	0	0	0	0	0	0	0 DR1	3.00E-03		0	0.003	0	0	0	0	0	0	0
Tz	0	0	-1	0	0	0	0	0	0 DR2	3.00E-03		0	0	0.003	0	0	0	0	0	0
Rx	0	0	0	-1	0	0	0	0	0 Dn	1.75E-03		0	0	0	0.00175	0	0	0	0	0
Ry	0	0	0	0	-1	0	0	0	0	1.75E-03		0	0	0	0	0	0.00175	0	0	0
Rz	0	0	0	0	0	0	-1	0	0	1.75E-03		0	0	0	0	0	0	0	0.00175	0
Df,p	0	0	0	0	0	0	0	0	0			0	0	0	0	0	0	0	0	0
DETECTOR												0	0	0	0	0	0	0	0	0

TX	TY	TZ	RX	RY	RZ	DM/M
0.008922	0.008922	0.091288	0.00480095	0.00480095	0.00175	0.059239
ABSOLUTE WORST CASE IMAGE REGISTRATION ERRORS DUE TO ASSEMBLY						

Ivory's ICs
x position and lens
elements' individual contributions

Worst case image registration
errors due to positioning and lens
tolerances. **AEH.**

Optomechanics

Example, *Unified* Nastran Model

Ivory produces a Nastran file with its “Unified” option.



```

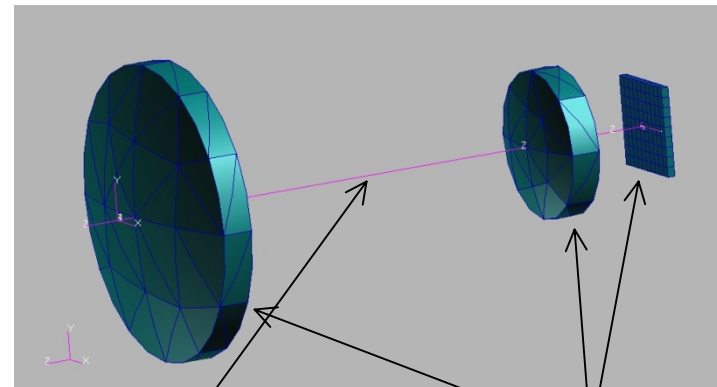
NASTRAN MESH
CEND
TITLE=DOUB'S IVORY(TM) UNIFIED OPTOMECHANICAL MODEL
$ SINGLE POINT CONSTRAINT SETS MUST BE CALLED OUT IN THE CASE CONTROL DECK.
SPC=1000
$ MULTIPOINT CONSTRAINT SETS MUST BE CALLED OUT IN THE CASE CONTROL DECK.
MPC=1000
BEGIN BULK
$ THE FOLLOWING GRID POINTS/DOFS HAVE BEEN ASSIGNED:
$ 1 THRU 2 /123456 ARE ASSIGNED TO THE OPTICAL ELEMENTS IN ASCENDING ORDER.
$ 3 /123456 ARE ASSIGNED TO THE SYSTEM DETECTOR.
$ 4 /123456 ARE ASSIGNED TO THE SYSTEM OBJECT.
$ 5 /123456 ARE ASSIGNED TO THE REGISTRATION VARIABLES TX, TY, TZ, RX, RY, RZ.
$ 6 /1 IS ASSIGNED TO THE REGISTRATION VARIABLE DM/M.
GRID 5 0. 0. 0.
GRID 6 0. 0. 0.
MPC 1000 5 1 -1. 1 1 1.3717
      1 5 -.2667 2 1 -.3717
      2 5 -.1286 3 1 -1.
MPC 1000 5 2 -1. 1 2 1.3717
      1 4 .2667 2 2 -.3717
      2 4 .1286 3 2 -1.
MPC 1000 5 3 -1. 1 3 1.8815
      2 3 -.8815 3 3 -1.
MPC 1000 5 4 -1. 1 4 1.3717
      2 4 -.3717 3 4 -1.
MPC 1000 5 5 -1. 1 5 1.3717
      2 5 -.3717 3 5 -1.
MPC 1000 5 6 -1. 3 6 -1.
.
.

```

Surf	Elem	Radius	Index	Thickness
1	obj	inf	AIR	inf
2	1	-3.5	ge	.25
3	1	-5.	AIR	2.67
4	2	-1.5	ge	.2
5	2	-1	AIR	.674
6	det	inf	AIR	0.0

MATERIAL	INDEX
AIR	1.0
ge	4.00024

Beginnings of the Nastran model:



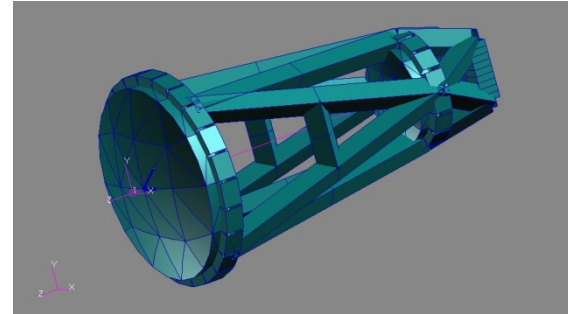
Optical elements from “.stp” files

Optomechanical Constraint Equations from *Ivory's* “Unified” option.

AEH.

Optomechanics

Rigid Body Check of a *Unified Model*



For unit displacements with an object at infinity ($f=4.741169$):

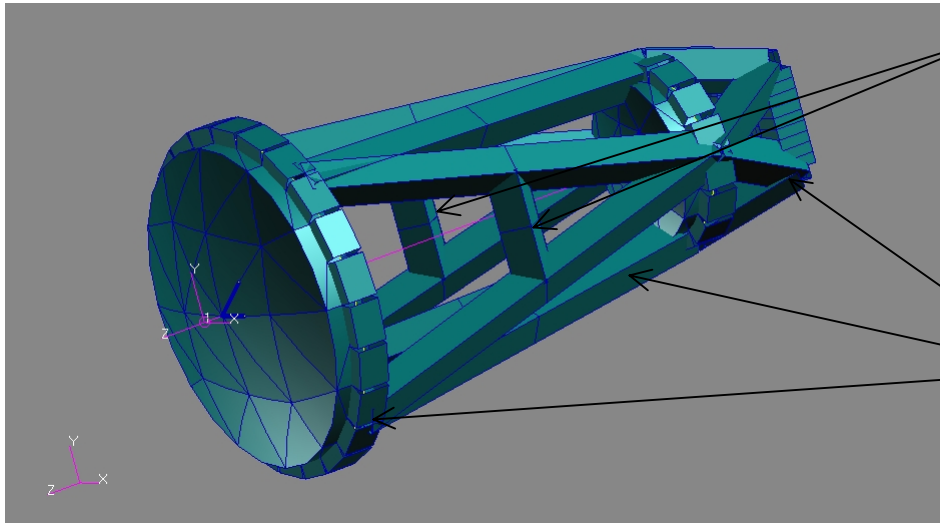
		D I S P L A C E M E N T V E C T O R						
POINT ID.	TYPE	T1	T2	T3	R1	R2	R3	
BASE MOTION:								
1.0 Tx	5 G	-1.239011E-10	9.571148E-12	-1.010361E-13	-1.980658E-13	-3.283262E-13	-9.969587E-12	
	6 G	3.545340E-14	0.0	0.0	0.0	0.0	0.0	
1.0 Ty	5 G	4.249783E-11	-8.842371E-12	5.046801E-13	4.182508E-13	4.095761E-13	-5.423809E-12	
	6 G	-2.176852E-13	0.0	0.0	0.0	0.0	0.0	
1.0 Tz	5 G	4.585644E-11	1.080863E-11	-1.085557E-12	-2.709695E-13	-6.882338E-13	8.544233E-13	
	6 G	4.827250E-13	0.0	0.0	0.0	0.0	0.0	
1.0 Rx	5 G	-8.676349E-11	-4.739557E+00	1.405411E-12	3.416156E-13	-1.469747E-12	1.259602E-11	
	6 G	7.719834E-13	0.0	0.0	0.0	0.0	0.0	
1.0 Ry	5 G	4.739557E+00	3.172970E-11	-9.775003E-13	-1.338907E-13	-3.279599E-13	1.546279E-12	
	6 G	4.457545E-13	0.0	0.0	0.0	0.0	0.0	
1.0 Rz	5 G	2.361326E-12	2.262890E-11	-3.414756E-13	-3.825188E-13	-9.552226E-14	-1.000000E+00	
	6 G	1.344123E-13	0.0	0.0	0.0	0.0	0.0	
REGISTRATION VARIABLES		TX	TY	TZ	RX	RY	RZ	
		DM/M						

Unified model accuracy = 0.99966

AEH.

Optomechanics

Unified Modeling Results



Mounting is at two points near the center of gravity.

Metering structure is a truss of square bars.

Displacements of the three optical elements are shown in blue.

Displacements of the image on the detector are shown in red.

SUBCASE 1

POINT ID.	TYPE	D I S P L A C E M E N T V E C T O R					
		T1	T2	T3	R1	R2	R3
1	G	2.522854E-07	8.796902E-03	-1.325016E-06	-2.856999E-03	-3.063985E-06	7.688029E-05
2	G	1.031466E-06	-4.884142E-04	6.866323E-07	-2.474126E-03	2.430291E-06	1.644103E-04
3	G	2.493282E-06	-2.096096E-03	-8.548020E-07	-2.529933E-04	-8.048320E-07	1.847545E-04
5	G	-2.025989E-06	1.326422E-02	-2.243482E-06	-4.693801E-04	-4.301375E-06	-1.847545E-04
6	G	1.931585E-06	0.0	0.0	0.0	0.0	0.0
7	G	6.786152E-05	-5.099613E-04	1.035619E-03	0.0	0.0	0.0
8	G	5.557859E-05	-3.271386E-04	8.008423E-04	0.0	0.0	0.0
9	G	7.444958E-05	-4.035432E-04	1.089830E-03	0.0	0.0	0.0
10	G	-6.545581E-05	-5.099232E-04	-1.034720E-03	0.0	0.0	0.0
11	G	-5.199726E-05	-3.248876E-04	-7.873403E-04	0.0	0.0	0.0
12							

DM/M of image

(the rest of the Nastran output file)

AEH.

Optomechanics

Unified Modeling Details in Excel

OPTOMECH- CONSTRAIN EQUATIONS (ABSOLUTE VALUES SMALLER THAN 0 ARE PRINTED AS 0.0)

REGISTRATION VARIABLES	TX	TY	TZ	RX	RY	RZ	DM/M	Df,p	LDesVar	Nastran Displacement Vector:	IMAGE MOTION CONTRIBUTIONS								
SYSTEM-OBJECT	Tx	0	0	0	0	0	0	0	0 Dt	0	0	0	0	0	0	0	0	0	0
	Ty	0	0	0	0	0	0	0	0 DR1	0	0	0	0	0	0	0	0	0	0
	Tz	0	0	0	0	0	0	0	0 DR2	0	0	0	0	0	0	0	0	0	0
	Rx	0	0	0	0	0	0	0	0 Dn	0	0	0	0	0	0	0	0	0	0
	Ry	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	Rz	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
	Df,p	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ELEMENT-1	Tx	1.3717	0	0	0	0	0	0	-1.5363 Dt	2.52E-07	3.461E-07	0	0	0	0	0	0	0	0
	Ty	0	1.3717	0	0	0	0	0	-3.0359 DR1	8.80E-03	0	0.0120667	0	0	0	0	0	0	0
	Tz	0	0	1.8815	0	0	0	-0.9602	1.357 DR2	-1.33E-06	0	0	-2.49E-06	0	0	0	0	1.272E-06	0
	Rx	0	0.2667	0	1.3717	0	0	0	-1.1841 Dn	-2.86E-03	0	-0.000762	0	-0.003919	0	0	0	0	0
	Ry	-0.2667	0	0	0	1.3717	0	0	0	-3.06E-06	8.172E-07	0	0	0	0	0	-4.2E-06	0	0
	Rz	0	0	0	0	0	0	0	0	7.69E-05	0	0	0	0	0	0	0	0	0
	Df,p	0	0	-1.8815	0	0	0	1.2495	0	0	0	0	0	0	0	0	0	0	0
ELEMENT-2	Tx	-0.3717	0	0	0	0	0	0	-3.0611 Dt	1.03E-06	-3.83E-07	0	0	0	0	0	0	0	0
	Ty	0	-0.3717	0	0	0	0	0	-3.1291 DR1	-4.88E-04	0	0.0001815	0	0	0	0	0	0	0
	Tz	0	0	0.8815	0	0	0	0.9602	5.5099 DR2	6.87E-07	0	0	-6.05E-07	0	0	0	0	6.593E-07	0
	Rx	0	0.1286	0	-0.3717	0	0	0	0.4251 Dn	-2.47E-03	0	-0.000318	0	0.0009196	0	0	0	0	0
	Ry	-0.1286	0	0	0	-0.3717	0	0	0	2.43E-06	-3.13E-07	0	0	0	0	0	-9.03E-07	0	0
	Rz	0	0	0	0	0	0	0	0	1.64E-04	0	0	0	0	0	0	0	0	0
	Df,p	0	0	-0.1381	0	0	0	0.2602	0	0	0	0	0	0	0	0	0	0	0
DETECTOR	Tx	-1	0	0	0	0	0	0	0 Dt	2.49E-06	-2.49E-06	0	0	0	0	0	0	0	0
	Ty	0	-1	0	0	0	0	0	0 DR1	-2.10E-03	0	0.0020961	0	0	0	0	0	0	0
	Tz	0	0	-1	0	0	0	0	0 DR2	-8.55E-07	0	0	8.548E-07	0	0	0	0	0	0
	Rx	0	0	0	-1	0	0	0	0 Dn	-2.53E-03	0	0	0	0.0025299	0	0	0	0	0
	Ry	0	0	0	0	-1	0	0	0	-8.05E-07	0	0	0	0	0	8.048E-07	0	0	0
	Rz	0	0	0	0	0	-1	0	0	1.85E-04	0	0	0	0	0	0	0	-0.000185	0
	Df,p	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Ivory's ICs
x Nastran's displacements =
elements' individual contributions

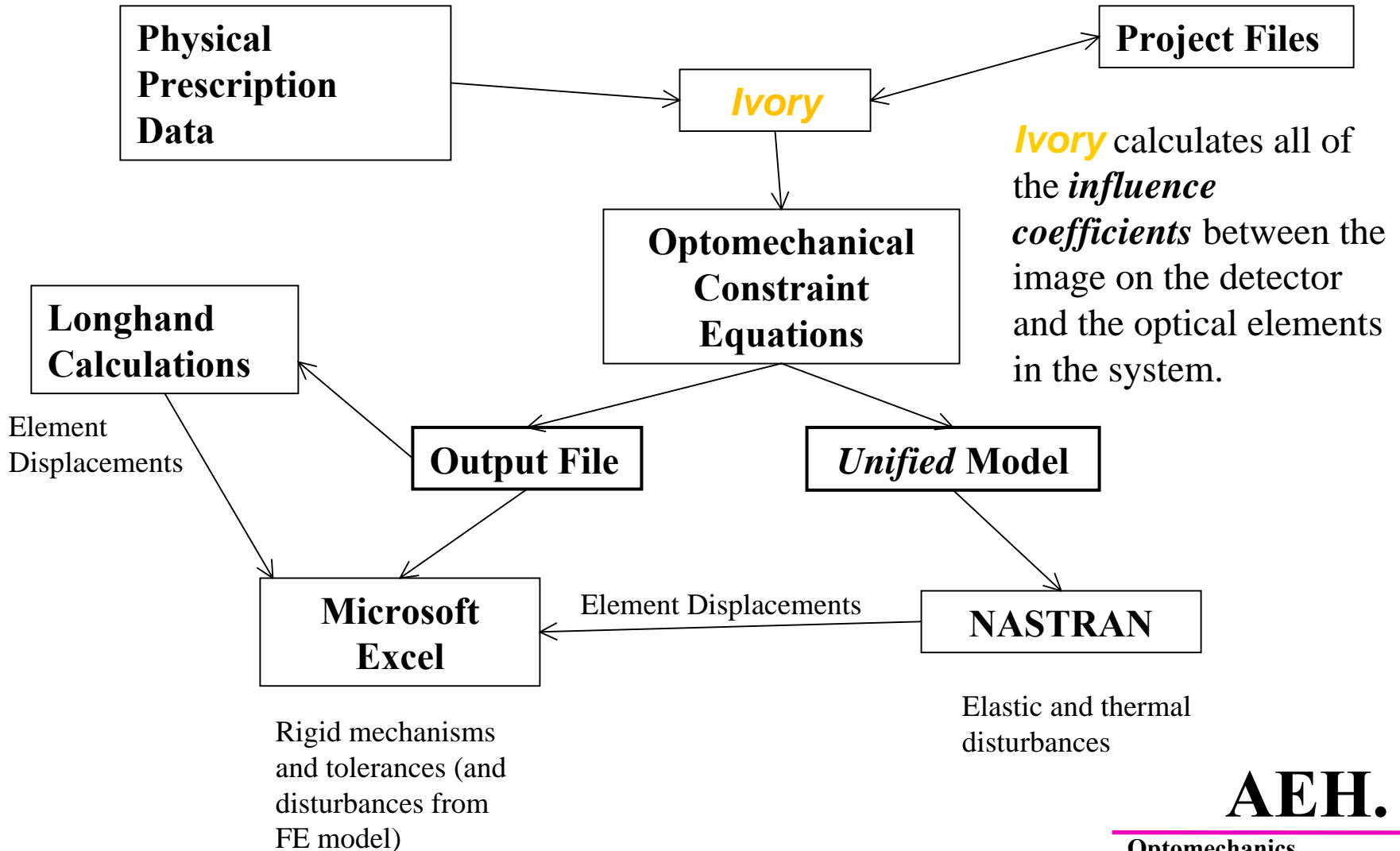
TX	TY	TZ	RX	RY	RZ	DM/M
-2.03E-06	0.0132642	-2.24E-06	-0.000469	-4.3E-06	-0.000185	1.932E-06
Image registration errors						

(Compare to Nastran on page 15)

AEH.

Optomechanics

Ivory Optomechanical Modeling Tools



AEH.

Optomechanics

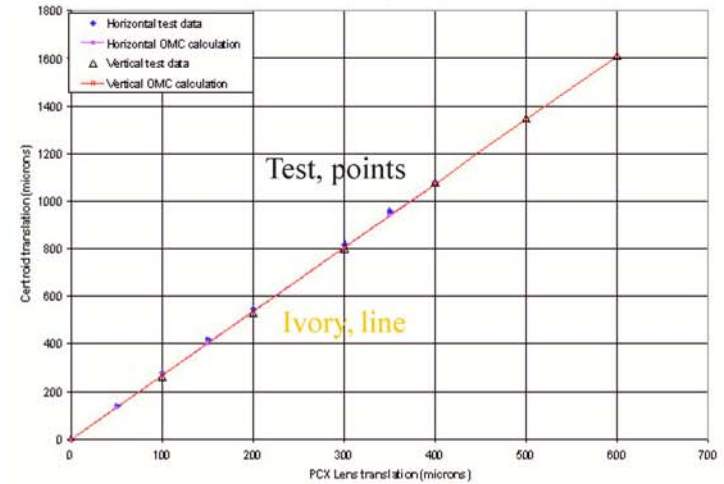
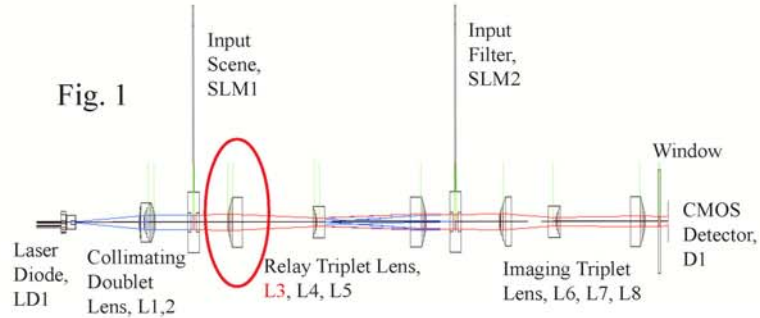
Ivory Applied to Align an Optical Image Correlator

AEH.

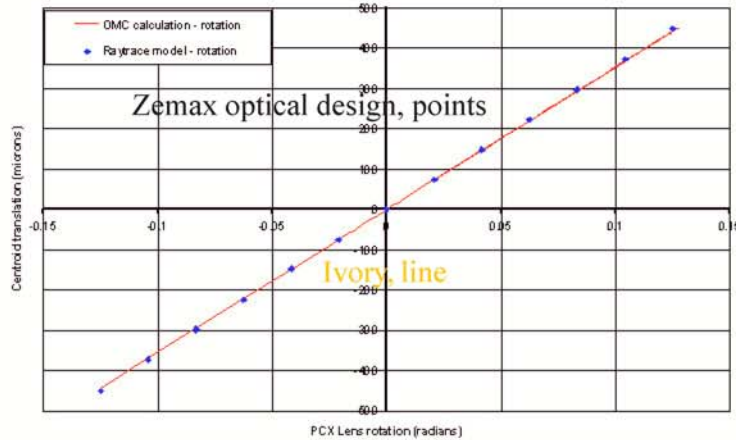
Optomechanics

AEH/Ivory Validation

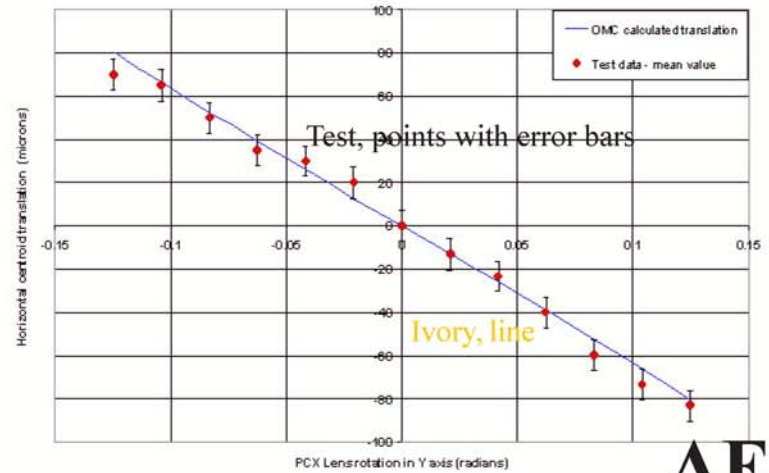
L3 T_x & T_y Translations



L3 R_x & R_y Rotations



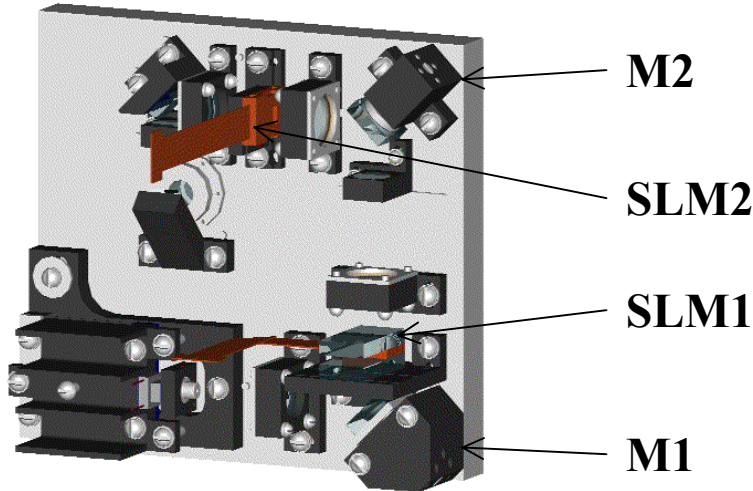
L3 Combined Translations & Rotations



AEH.

Optomechanics

Aligning Spatial Light Modulators



Requirement:
Align the image of SLM1 on SLM2 to less than 0.1 pixel (1.5μ) in Tx, Ty and Rz.

Tx															
Ty			0.0184	-176.8							1.083	-37.6			-26.6
Tz			-0.00024								-0.829				
Rx				0.026								-1.53			
Ry					0.018										1.083
Rz					1.414										1.414
DM/M			0.000208									-0.031			
Registration Variables	Tx	Ty	Tz	Rx	Ry	Rz		Tx	Ty	Tz	Rx	Ry	Rz		
			M1 Motions								M2 Motions				

Required:

Stroke, mr (\pm)
Resolution, μ r (\pm)

(Rx Ry)
8.5 11.1
8.5 12.

(Rx Ry)
42.
589.

Achieved:

Stroke, mr (\pm)
Resolution, μ r (\pm)

17. **17.**
0.26 **0.26**

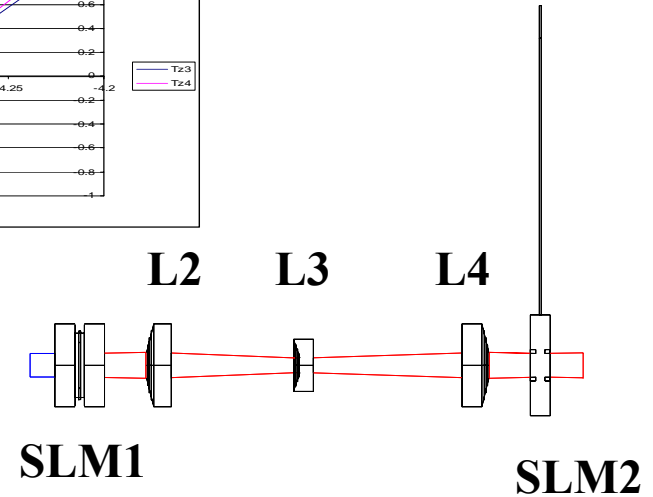
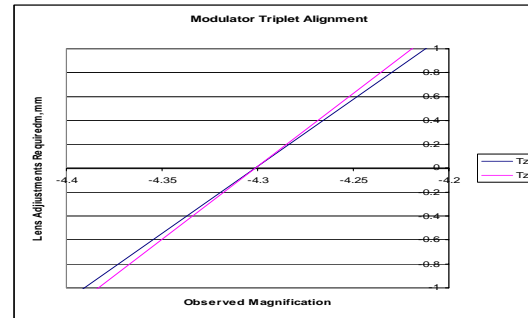
52. **52.**
556. **556.**

AEH.

Optomechanics

Scaling the Diffracted Light

Requirement:
Align the image focus and numerical aperture at SLM2 using lenses 3 and 4.



Registration Variables

Tx	-2.68			3.54			1.91			0.52				
Ty		2.68		3.54				-1.91		0.52				
Tz			7.14				-7.21		-6.55				-3.63	
Rx				2.68						-1.91				
Ry					-2.68						1.91			
Rz														
DM/M			0.0335				-0.0081		-0.0117				0.0301	
	Tx	Ty	Tz	Rx	Ry	Rz	Df	Tx	Ty	Tz	Rx	Ry	Rz	Df
			L3 Motions							L4 Motions				

AEH.

Optomechanics

Ivory Applied to Align an Optical Image Correlator

Designed alignment mirrors
Designed alignment charts

Reduced assembly time by 2/3
Reduced electrical power by 3/4

AEH.

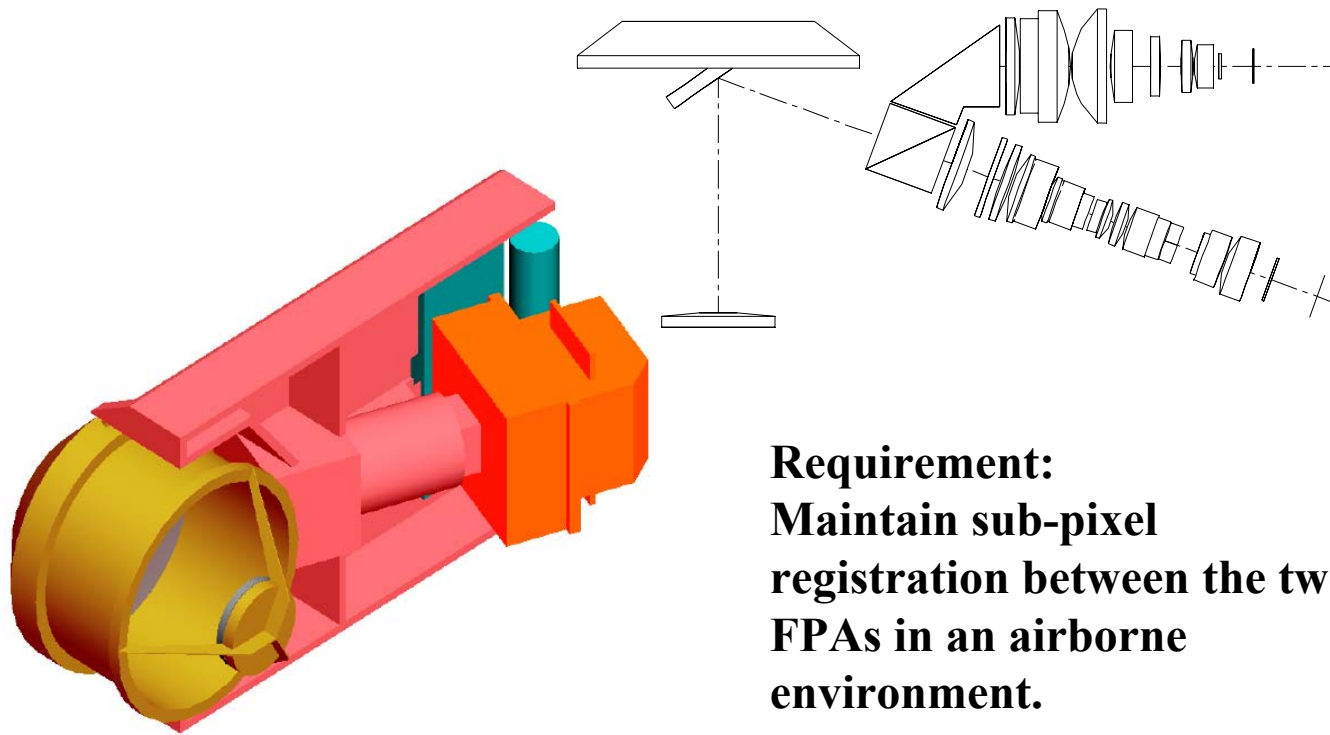
Optomechanics

Ivory Applied to Register Images in a Two-color Camera

AEH.

Optomechanics

A Two-color Camera

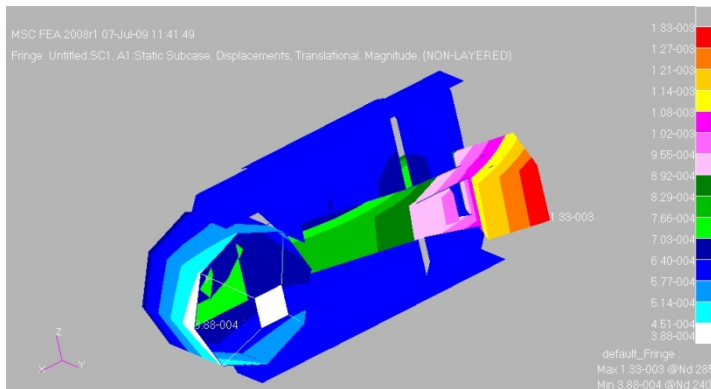
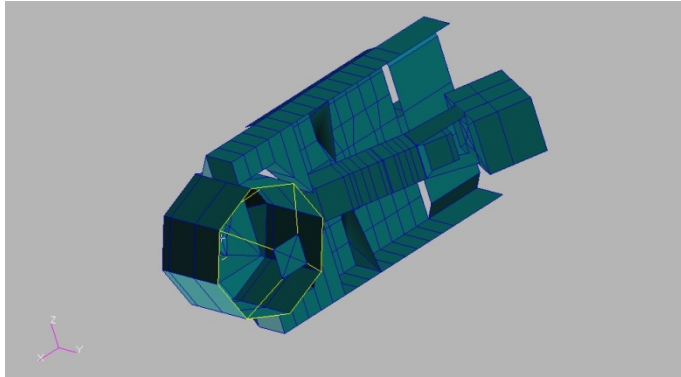


**Requirement:
Maintain sub-pixel
registration between the two
FPAs in an airborne
environment.**

AEH.

Optomechanics

FE Analysis of Element Displacements



1.5 GS ALONG THE X (ROLL) AXIS

NODE	X TRANS	Y TRANS	Z TRANS	X ROT	Y ROT	Z ROT
1	-7.4365E-04	2.7726E-06	6.7300E-07	3.2085E-07	-4.6245E-05	-2.1854E-05
2	-4.5475E-04	-2.0027E-05	4.1551E-06	3.0762E-07	-1.1534E-07	-4.8295E-05
3	-8.0244E-04	8.8353E-06	8.6687E-08	2.8875E-05	2.3929E-05	-5.5360E-05
4	-7.0552E-04	2.5088E-04	-1.8926E-07	-1.3864E-06	4.8634E-07	3.9087E-05
5	-7.2517E-04	1.9579E-04	-2.7311E-07	-1.3896E-06	4.9393E-07	3.9220E-05
6	-7.6405E-04	8.9584E-05	-4.8932E-07	-1.7689E-06	4.3251E-07	3.9460E-05
7	-7.7197E-04	6.7650E-05	-6.5347E-07	-2.2127E-06	5.6940E-07	3.9213E-05
8	-7.7667E-04	5.2098E-05	-1.0905E-06	-1.3148E-06	-1.5381E-07	4.0670E-05
9	-7.8787E-04	2.2585E-05	-1.4003E-06	-1.5766E-07	-2.3795E-07	4.0344E-05
10	-7.9793E-04	-3.4134E-06	-1.5584E-06	-7.2602E-08	-2.6334E-07	4.0037E-05
11	-8.1214E-04	-4.0650E-05	-1.7627E-06	5.8725E-08	-3.6616E-07	4.0027E-05
12	-8.2012E-04	-6.1790E-05	-1.8442E-06	2.9572E-09	-4.1944E-07	4.0000E-05
13	-8.1836E-04	-5.6886E-05	-1.8126E-06	2.8440E-07	-5.1638E-07	3.9998E-05
14	-8.3497E-04	-1.0156E-04	-2.0556E-06	6.4894E-07	-5.2880E-07	4.0136E-05
15	-8.4091E-04	-1.1746E-04	-2.1336E-06	7.5641E-07	-5.8834E-07	4.0202E-05
16	-8.5049E-04	-1.4312E-04	-2.2435E-06	8.0778E-07	-6.3497E-07	4.0292E-05
17	-8.5774E-04	-1.6249E-04	-2.3040E-06	8.6741E-07	-6.8204E-07	4.0442E-05
18	-8.6771E-04	-1.8889E-04	-2.4746E-06	1.3983E-06	-7.3197E-07	4.0482E-05
19	-8.6854E-04	-1.9125E-04	-2.5160E-06	1.4982E-06	-7.9809E-07	4.0476E-05
20	-8.7789E-04	-2.2005E-04	-2.5080E-06	1.5741E-06	-9.9234E-07	4.0512E-05
21	-9.1048E-04	-3.0888E-04	-3.1540E-06	1.6964E-06	-7.8557E-07	4.0388E-05
22	-9.1807E-04	-3.2971E-04	-3.2335E-06	1.6898E-06	-8.4878E-07	4.0404E-05
23	-9.5055E-04	-3.9985E-04	-3.9234E-06	1.7104E-06	-8.2646E-07	4.5268E-05
24	-5.9238E-04	1.2553E-04	3.9390E-06	-1.2148E-06	-3.2840E-07	3.8068E-05
25	-5.9515E-04	3.5638E-05	3.2778E-06	-2.6629E-06	-9.5080E-08	3.8707E-05
26	-5.9357E-04	-2.5492E-05	3.8154E-06	-1.2173E-06	1.6194E-07	3.7504E-05
27	-5.9332E-04	-5.0600E-05	4.0013E-06	-1.4054E-06	1.7431E-07	3.7292E-05
28	-5.9335E-04	-7.6025E-05	4.2174E-06	-1.5854E-06	2.0532E-07	3.7178E-05
29	-5.9271E-04	-1.7649E-04	5.2699E-06	-2.3304E-06	3.5810E-07	3.6830E-05
30	-5.9298E-04	-2.0618E-04	5.5929E-06	-2.2995E-06	4.2450E-07	3.6836E-05
31	-5.9109E-04	-2.8380E-04	6.3397E-06	-2.2851E-06	6.0361E-07	3.6382E-05
32	-9.0787E-04	-3.7085E-04	3.8561E-06	-1.1076E-06	1.8081E-09	-8.6392E-05
33	-9.0780E-04	-2.3755E-04	3.8588E-06	-1.0989E-06	1.8059E-09	-8.6393E-05
34	-9.0755E-04	-5.1807E-05	3.8634E-06	-1.0885E-06	1.7708E-09	-8.6599E-05

AEH.

Optomechanics

Ivory Applied to Register Images in a Two-color Camera

Calculated dynamic boresight error between two optical paths

**Operational boresight stability would be *problematic*
(verified in flight tests)**

AEH.

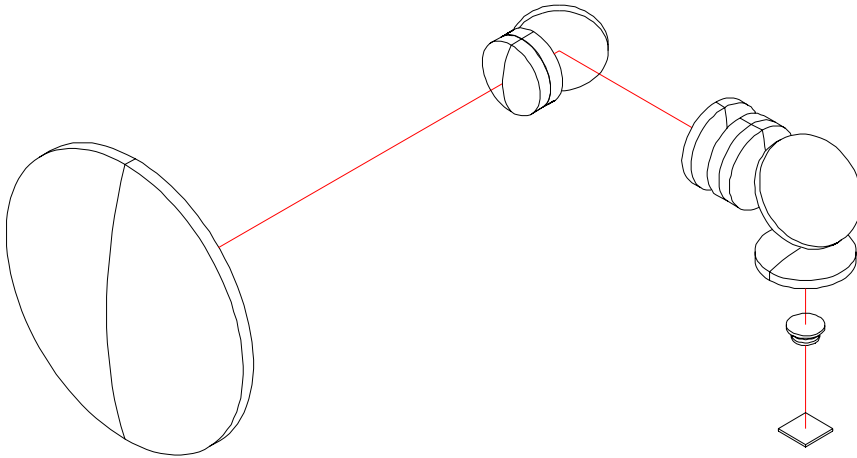
Optomechanics

Ivory Applied to Stabilize a Mid-wavelength FLIR

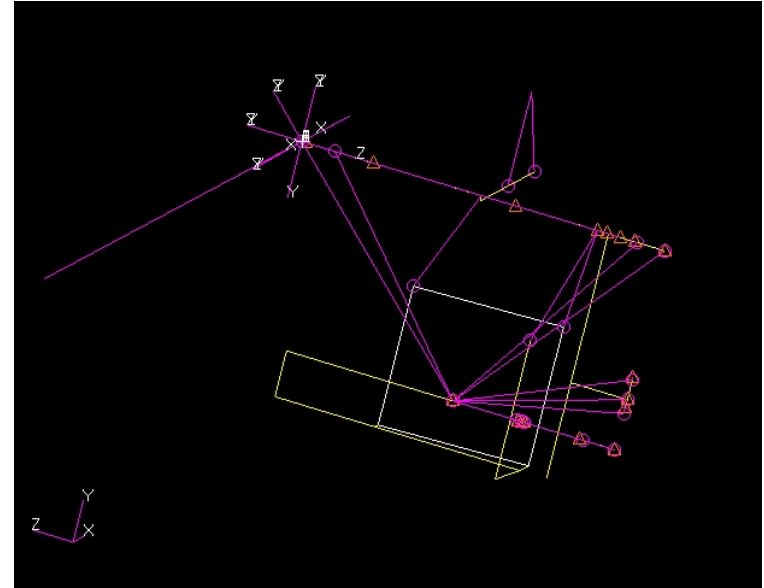
AEH.

Optomechanics

A Mid-wavelength FLIR



The task:
Verify that the line of sight will be stable to less than $10 \mu\text{r}$ rms in thermal extremes and random vibration environment.



The method:
A simple (but carefully constructed) beam-element **Nastran** model with lumped masses for the lenses and **Ivory's** influence coefficients driving the image motions.

AEH.

Optomechanics

Thermal Image Stability in Nastran

```

NASTRAN MESH
CEND
TITLE=NF'S IVORY(TM) UNIFIED OPTOMECHANICAL MODEL
$ SINGLE POINT CONSTRAINT SETS MUST BE CALLED OUT IN THE CASE CONTROL DECK.
SPC=1000
$ MULTIPOINT CONSTRAINT SETS MUST BE CALLED OUT IN THE CASE CONTROL DECK.
MPC=1000
BEGIN BULK
$ THE FOLLOWING GRID POINTS/DOFS HAVE BEEN ASSIGNED:
$ 1 THRU 12 /123456 ARE ASSIGNED TO THE OPTICAL ELEMENTS IN ASCENDING ORDER.
$ 13 /123456 ARE ASSIGNED TO THE SYSTEM DETECTOR.
$ 14 /123456 ARE ASSIGNED TO THE SYSTEM OBJECT.
$ 15 /123456 ARE ASSIGNED TO THE REGISTRATION VARIABLES TX, TY, TZ, RX, RY, RZ.
$ 16 /1 IS ASSIGNED TO THE REGISTRATION VARIABLE DM/M.
GRID 15 0. 0. 0.
GRID 16 0. 0. 0.
MPC 1000 15 1 -1. 1 1 -2.28034
      1 5 .51305 2 1 -.51904
      2 5 3.2867 3 1 1.62407
      3 5 .15684 4 5 -2.45353
      5 1 -1.382265 5 .03296
      6 1 2.114816 5 -.2064
      7 1 -1.347517 5 -.09949
      8 5 -3.347539 1 1.56036
      9 5 -.13952 10 5 -.01585
     11 5 -.01503 12 5 -.01585
     13 1 -1.
MPC 1000 15 2 -1. 1 2 -2.28034
      1 4 -.51305 2 2 -.51904
      2 4 -3.2867 3 2 1.62407
      3 4 -.15684 4 3 -1.66214

```

DISPLACEMENT VECTOR

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
125	G	2.600000E-05	-5.811000E-05	-2.562690E-05	-6.987358E-18	-1.024498E-18	4.521079E-19
126	G	2.600000E-05	-5.811000E-05	-6.511700E-06	-6.913750E-18	-9.915638E-19	4.521079E-19
151	G	0.0	0.0	0.0	0.0	0.0	0.0
152	G	7.800000E-05	-5.158406E-20	2.499171E-18	-3.257421E-18	-3.933409E-19	5.972928E-20
1000	G	5.200000E-09	-4.404351E-09	3.450281E-03	-1.333385E-18	-1.452332E-18	-7.63793E-19
1001	G	-2.206333E-03	0.0	0.0	0.0	0.0	0.0
2011	G	1.444440E-06	0.0	0.0	0.0	0.0	0.0
2012	G	-2.606998E-05	0.0	0.0	0.0	0.0	0.0
2013	G	-7.711902E-05	0.0	0.0	0.0	0.0	0.0

AEH.

Optomechanics

Thermal Image Stability in Excel

(Bottom of *Ivory's* *.out file in Excel)

Tx	0	0	0	0	0	0	0	0.3964	Dt	0	TX
Ty	0	0	0	0	0	0	0	0	DR1	5.811E-05	TY
Tz	0	0	0	0	0	0	0	0	DR2	7.892E-05	TZ
Rx	0	-0.0159	0	0	0	0	0	0.0146	Dn		RX
Ry	-0.0159	0	0	0	0	0	0	0			RY
Rz	0	0	0	0	0	0	0	0			RZ
Df,p	0	0	-1	0	0	0	0	0		1.401E-07	Df,p
ELEMENT-12											
Tx	-1	0	0	0	0	0	0	0	Dt	0	TX
Ty	0	-1	0	0	0	0	0	0	DR1	5.811E-05	TY
Tz	0	0	-1	0	0	0	0	0	DR2	5.981E-05	TZ
Rx	0	0	0	-1	0	0	0	0	Dn		RX
Ry	0	0	0	0	-1	0	0	0			RY
Rz	0	0	0	0	0	-1	0	0			RZ
Df,p	0	0	0	0	0	0	0	0			Df,p
DETECTOR											

0 -9.73129E-09 0.00345025 0 0 0 -0.00220631
 TX TY TZ RX RY RZ DM/M

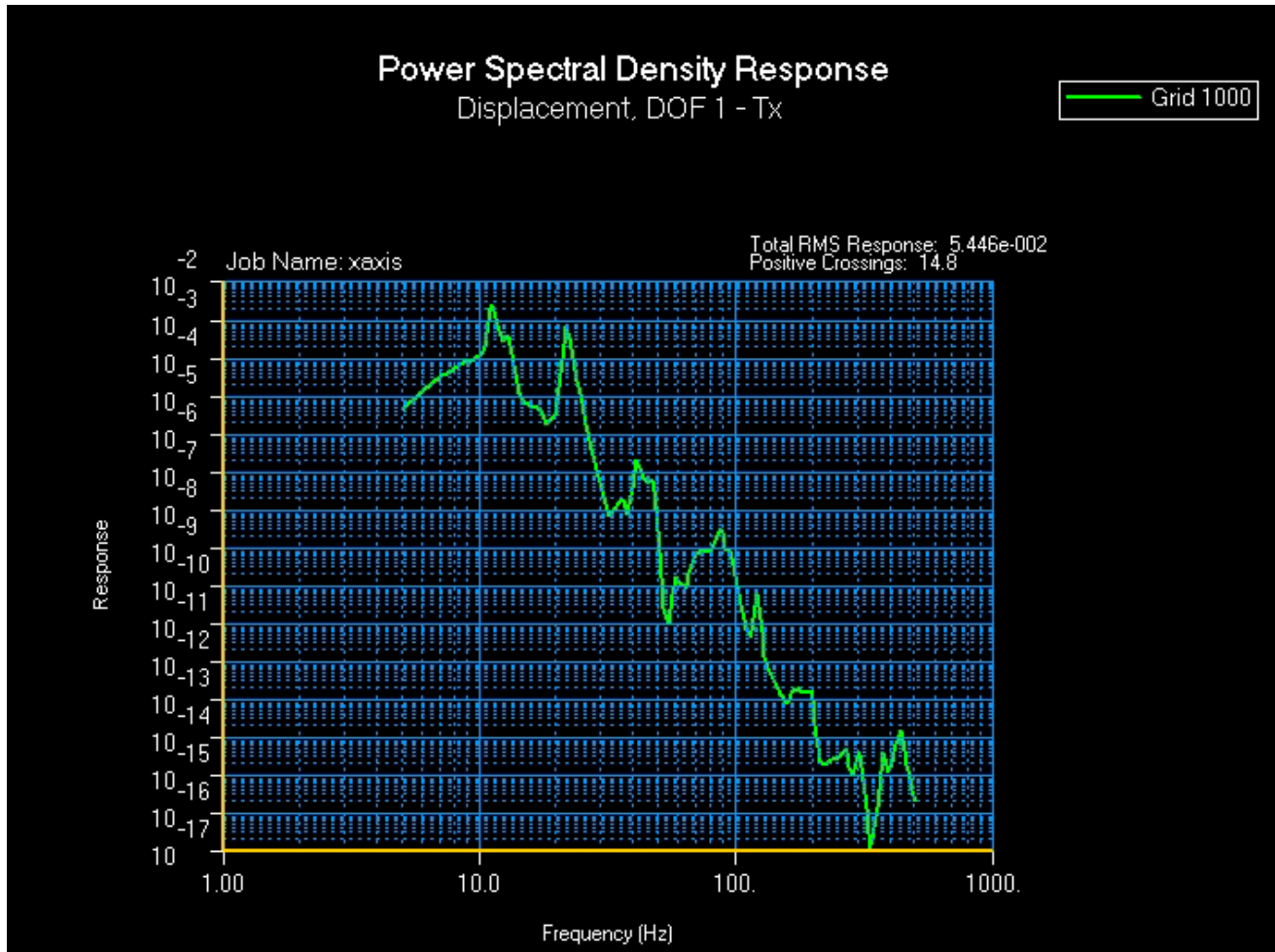
REGISTRATION ERRORS PER DEGREE F

Compare to Nastran on previous page

AEH.

Optomechanics

Dynamic Image Response in Nastran



AEH.

Optomechanics

Dynamic Image Stability in Nastran

NASTRAN modeling:

Model Comparison	Mass Lb	CG, in. (ProE coordinate system)		
		X	Y	Z
ProE	4.97	-2.53	-2.3	0.98
NASTRAN	4.74	-2.47	-2.84	0.52

(Balasted by increasing the density of the Albetmet)

NASTRAN modeling parameters:

Fundamental resonance:	425	Hz
Structural damping:	0.05	
Pass-band:	5 to 500	Hz
Structural material:	Albetmet	

NASTRAN results.

Vibration Excitation Axis:	X	Y	Z
Registration Variables:	RMS response of image at the detector:		
Tx	5.31E-06	1.50E-07	8.27E-07
Ty	2.43E-08	1.51E-06	2.37E-06
Tz	9.53E-07	2.11E-06	1.25E-06
Rx	1.05E-07	7.34E-09	3.75E-08
Ry	7.41E-07	5.65E-08	2.97E-07
Rz	5.56E-07	3.13E-08	1.65E-07
DM/M	1.15E-08	1.34E-06	3.66E-07

Units: inches, radians

7 microradians equivalent RMS image motion:	Margins of Safety:		
	X	Y	Z
0.000138	25.0	915.8	165.8
0.000138	5668.2	90.6	57.3

AEH.

Optomechanics

Ivory Applied to Stabilize a Mid-wavelength FLIR

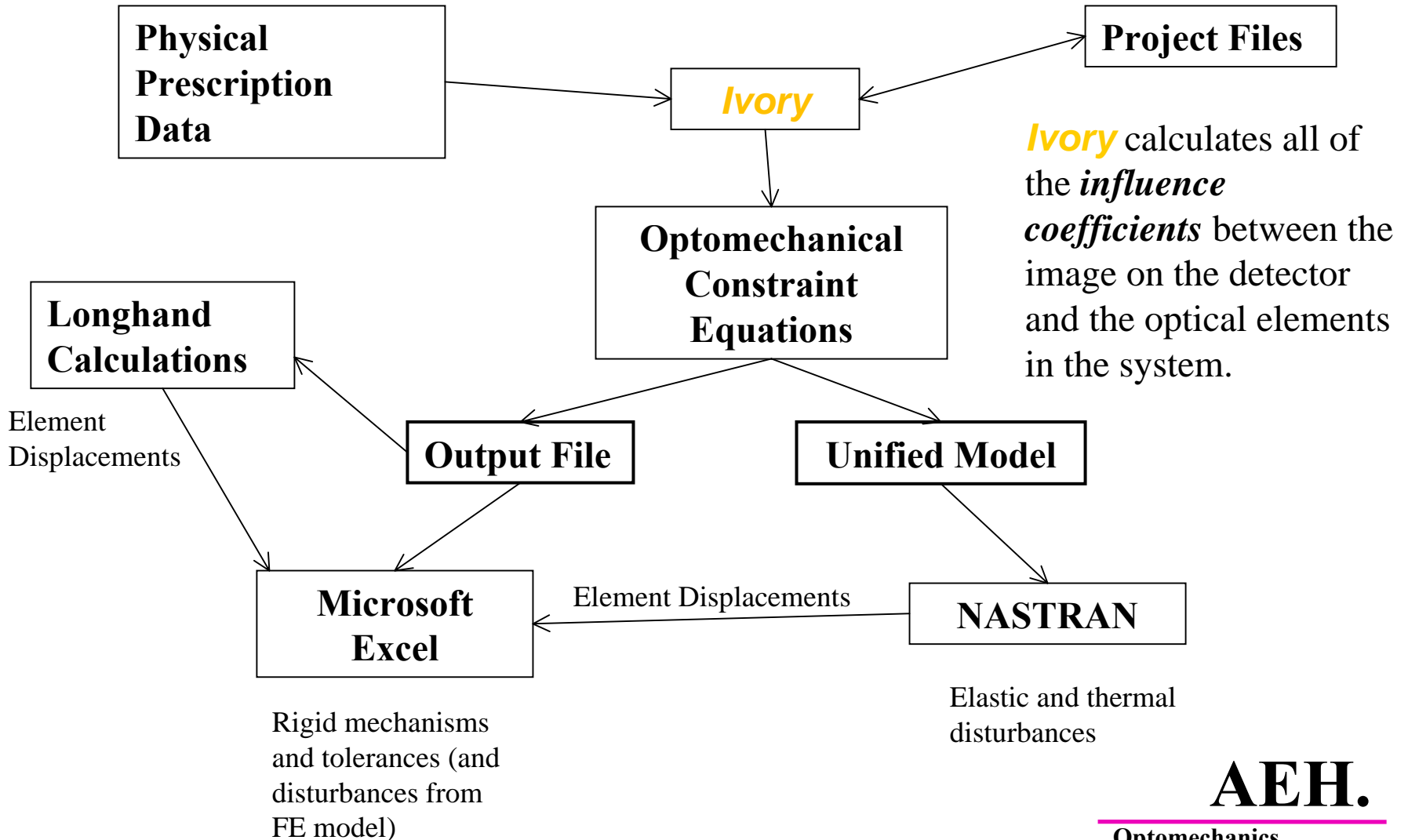
Analyzed the image's thermal stability
Analyzed image's rms jitter in random vibration

**Large margins of safety in both analyses
(verified in flight tests)**

AEH.

Optomechanics

Ivory Optomechanical Modeling Tools



AEH.

Optomechanics

Ivory Optomechanical Modeling Tools

Ivory provides *quantitative* answers to challenges in

Tolerancing
Alignment
Rigid mechanisms
Elastic structures
Thermal distortion
Environmental sensitivity
Image stability
and much, much more.

AEH.

Optomechanics