

Tutorial 4

Optomechanical Static Analysis

In this tutorial we shall:

Prepare an **Ivory** optomechanical model from a telescope's optical prescription

Evaluate the optical faithfulness of the model in **Ivory's** output file

Import the **Ivory** optomechanical model into **Patran**

Import the CAD models of the optical elements into **Patran**

Attach the optomechanical model to the meshed optical elements in **Patran**

Construct lens cells in **Patran**

Construct a structural truss in **Patran** to support the lens cells

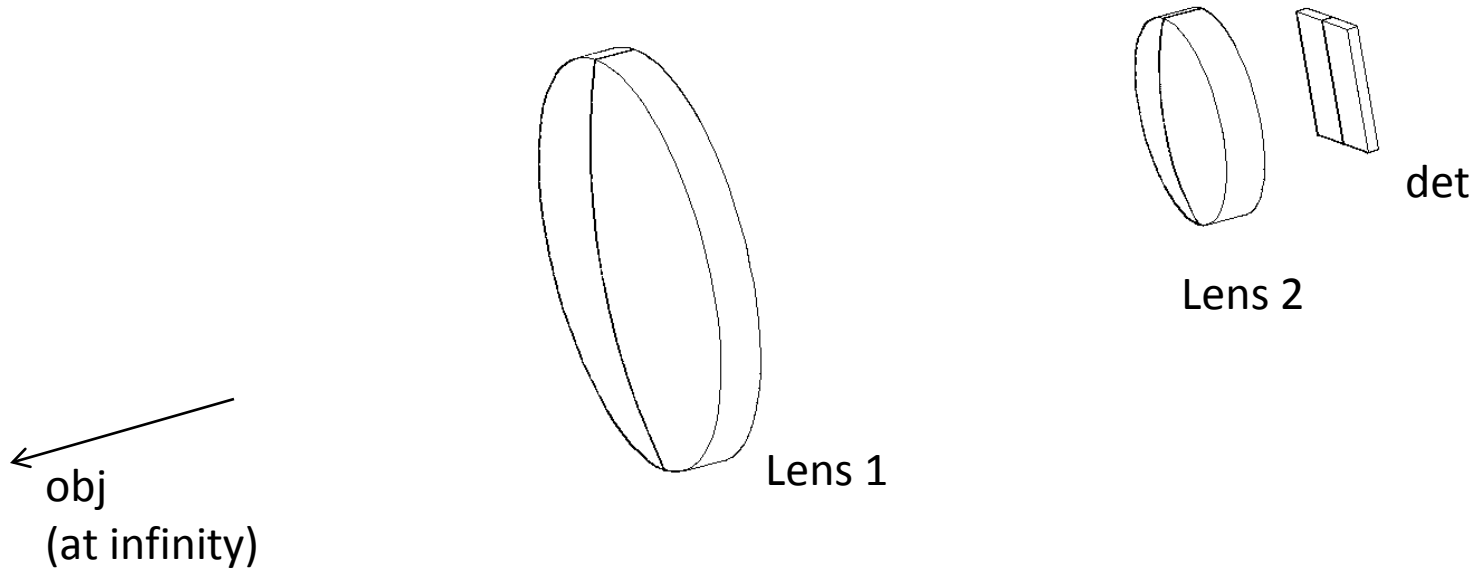
Checkout the full model's optical quality with 6 DOF rigid body checks in **Nastran**

Analyze the static gravity stability of the image on the detector in **Nastran**

AEH.

Optomechanics

The Telescope's Optical Geometry Data



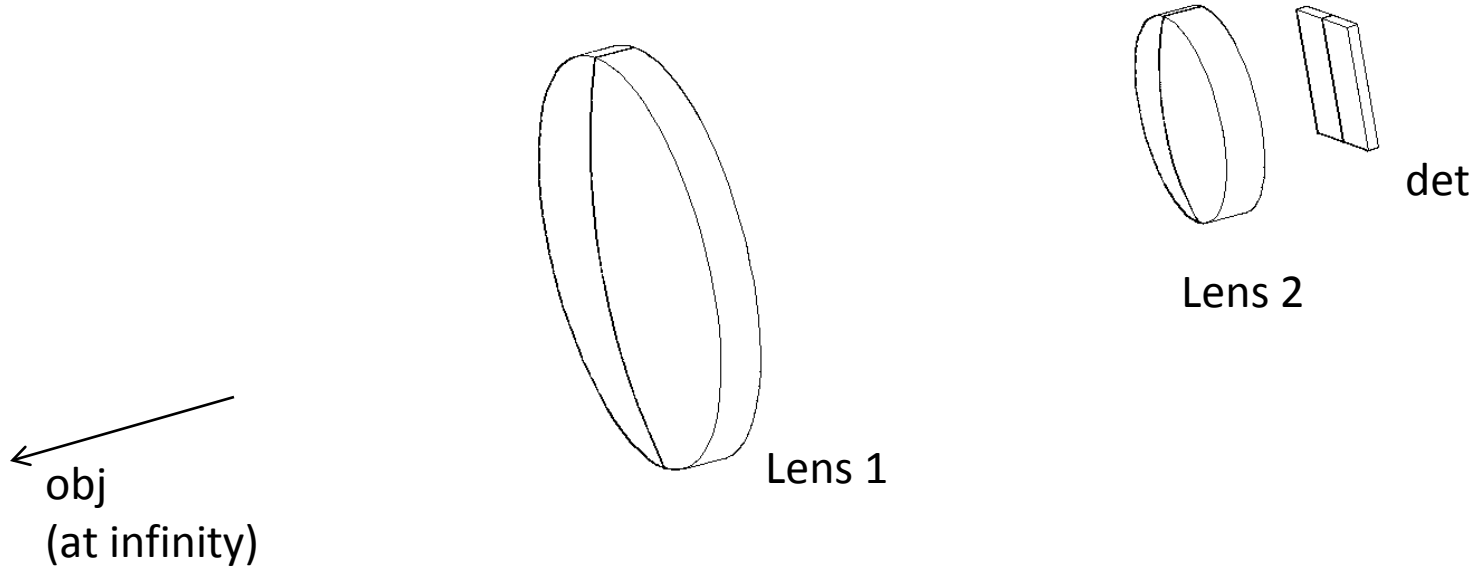
Surf	Elem	Radius	Index	Thickness
1	obj	inf	AIR	inf
2	1	3.5	ge	.25
3	1	5.	AIR	2.67
4	2	1.5	ge	.2
5	2	1	AIR	.674
6	det	inf	AIR	0.0

We shall call this file “tele.dat”

AEH.

Optomechanics

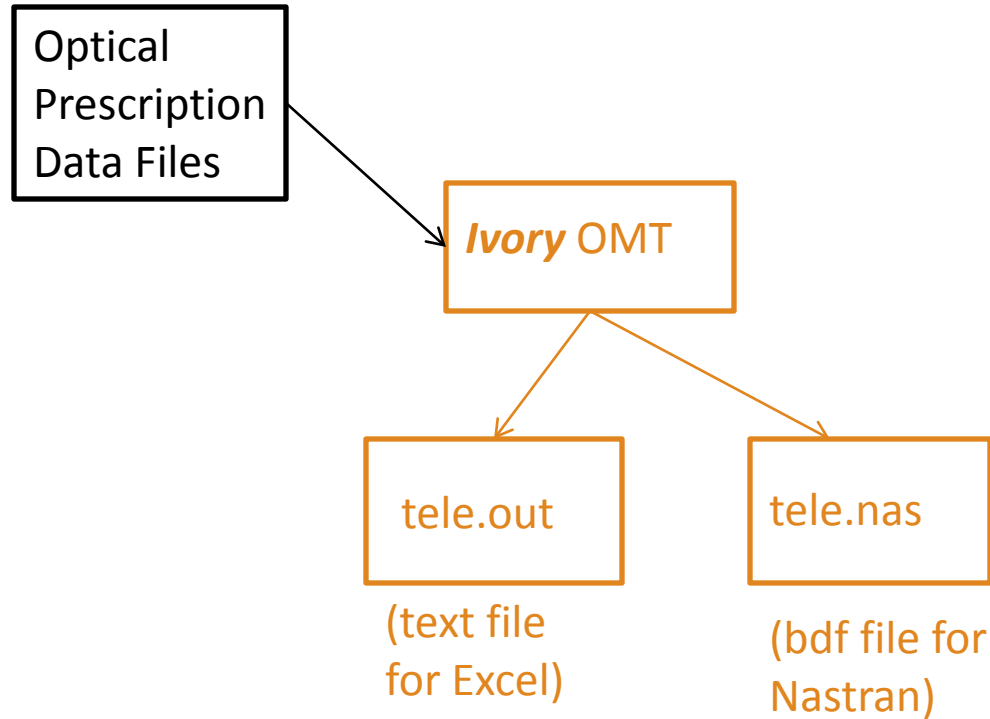
The Telescope's Index of Refraction Data



MATERIAL	INDEX
AIR	1.0
ge	4.00024

We shall call this file “tele.ind”

Ivory Generates the *Unified Models*' Data Files



AEH.

Optomechanics

At the Top of the tele.out File for Excel:

Check the optical properties reported by Ivory

Output from -

IVORY Optomechanical Modeling Tools

Version 3.0

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PROJECT NAME: 'TELE' TIME AND DATE: 11:29:55 11-20-2014

PHYSICAL PRESCRIPTION INPUT ECHO IN OPTICAL CONVENTIONS

Surf	Elem	Radius	Index	Thickness	Type	f1	f2	f3	f4
1	obj	inf	1.0	inf	obj	1	1	0	0
2	1	3.5	4.00024	.25	LENS	0	0	0	0
3	1	5	1.0	2.67	LENS	0	0	0	0
4	2	1.5	4.00024	.2	LENS	0	0	0	0
5	2	1	1.0	.674	LENS	0	0	0	0
6	det	inf	1.0	0	det				

INDEXES OF REFRACTION ARE RELATIVE TO THE VALUE OF 1.000292.

Check the data echos.

PHYSICAL PRESCRIPTION INPUT ECHO IN MECHANICAL CONVENTIONS

Surf	Elem	Radius	Index	Thickness	Type	f1	f2	f3	f4
1	obj	inf	1.0	inf	obj	1	0	0	0
2	1	-3.5	4.00024	.25	LENS	0	0	0	0
3	1	-5	1.0	2.67	LENS	0	0	0	0
4	2	-1.5	4.00024	.2	LENS	0	0	0	0
5	2	-1	1.0	.674	LENS	0	0	0	0
6	det	inf	1.0	0	det				

INDEXES OF REFRACTION ARE RELATIVE TO THE VALUE OF 1.000292.

GAUSSIAN PRESCRIPTION

ELE	F	H1	H2	P	P/AIR	PHI	THETA	TYPE	PHI'
obj	inf	0	0	0	inf	0	0	obj	
1	3.4565059	.12962156	.18517366	.1944479	3.0694484	0	0	LENS	
2	-1.4284694	-.21427469	-.1428498	.1285751	.5311502	0	0	LENS	
det	inf	0	0	0	0	0	0	det	
SYSTEM	4.741172	10.317298	4.0674085	9.3698891	4.7414085				

Focal length agrees with optical design.

OBJECTS, IMAGES AND MAGNIFICATIONS

ELE	F	S	S'	M	PHI	THETA	TYPE	e/Tzo	PHI'
obj	inf	0	0	1.0	0	0	obj	0	0
1	3.456506	0	-3.456506	0	0	0	LENS	0	0
2	-1.428469	-.3870576	.5309138	1.371666	0	0	LENS	-.9602	0
det	inf	2.36431E-4	2.36431E-4	+1.0	0	0	det	0	0

Focus error is very small.

AEH.

At the Bottom of the tele.out File for Excel:

Check the Influence coefficients with “validation sums.”

OPTOMECHANICAL CONSTRAINT EQUATIONS (ABSOLUTE VALUES SMALLER THAN 0 ARE PRINTED AS 0.0)

	REGISTRATION VARIABLES								
	TX	TY	TZ	RX	RY	RZ	DM/M	Df,p,G	LDesVar
Tx	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Dt
Ty	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	DR1
Tz	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	DR2
Rx	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Dn
Ry	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Rz	0.0	0.0	0.0	0.0	0.0	1	0.0	0.0	
Df,p,G	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
SYSTEM-OBJECT									
Tx	1.371666	0.0	0.0	0.0	0.0	0.0	0.0	-1.536252	Dt
Ty	0.0	1.371666	0.0	0.0	0.0	0.0	0.0	-3.035868	DR1
Tz	0.0	0.0	1.881468	0.0	0.0	0.0	-.9602349	1.356994	DR2
Rx	0.0	.2667176	0.0	1.371666	0.0	0.0	0.0	-1.184077	Dn
Ry	-.2667176	0.0	0.0	0.0	1.371666	0.0	0.0	0.0	
Rz	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Df,p,G	0.0	0.0	-1.881468	0.0	0.0	0.0	1.249544	0.0	
ELEMENT-1									
Tx	-.3716662	0.0	0.0	0.0	0.0	0.0	0.0	-3.061093	Dt
Ty	0.0	-.3716662	0.0	0.0	0.0	0.0	0.0	-3.129063	DR1
Tz	0.0	0.0	-.8814681	0.0	0.0	0.0	.9602349	5.509846	DR2
Rx	0.0	.1285751	0.0	-.3716662	0.0	0.0	0.0	.4251073	Dn
Ry	-.1285751	0.0	0.0	0.0	-.3716662	0.0	0.0	0.0	
Rz	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Df,p,G	0.0	0.0	-.1381358	0.0	0.0	0.0	.2601849	0.0	
ELEMENT-2									
Tx	-1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Dt
Ty	0.0	-1	0.0	0.0	0.0	0.0	0.0	0.0	DR1
Tz	0.0	0.0	-1	0.0	0.0	0.0	0.0	0.0	DR2
Rx	0.0	0.0	0.0	-1	0.0	0.0	0.0	0.0	Dn
Ry	0.0	0.0	0.0	0.0	-1	0.0	0.0	0.0	
Rz	0.0	0.0	0.0	0.0	0.0	-1	0.0	0.0	
Df,p,G	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
DETECTOR									

Thank you for using IVORY(tm) to prepare the Optomechanical Constraint Equations for 'TELE'.

Sums =	-0.0000002	-0.0000002	-0.0000001	-0.0000002	-0.0000002	0.0
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The sums of the diagonal terms should be computational zeros. OK.

AEH.

Optomechanics

The tele.nas Bulk Data File (in Two Columns) for Nastran is:

Compare these values to tele.out

```

NASTRAN MESH
CEND
TITLE=TELE'S IVORY(TM) UNIFIED OPTOMECHANICAL MODEL
$ SINGLE POINT CONSTRAINT SETS MUST BE CALLED OUT IN THE CASE CONTROL DECK.
SPC=1000
$ MULTIPOINT CONSTRAINT SETS MUST BE CALLED OUT IN THE CASE CONTROL DECK.
MPC=1000
BEGIN BULK

$ THE FOLLOWING GRID POINTS/DOFS HAVE BEEN ASSIGNED:
$ 1 THRU 2 /123456 ARE ASSIGNED TO THE OPTICAL ELEMENTS IN ASCENDING ORDER.
$ 3 /123456 ARE ASSIGNED TO THE SYSTEM DETECTOR.
$ 4 /123456 ARE ASSIGNED TO THE SYSTEM OBJECT.
$ 5 /123456 ARE ASSIGNED TO THE REGISTRATION VARIABLES TX, TY, TZ, RX, RY, RZ.
$ 6 /1 IS ASSIGNED TO THE REGISTRATION VARIABLE DM/M.

GRID 5 0. 0. 0.
GRID 6 0. 0. 0.

MPC 1000 5 1 -1. 1 1 1.371666
      1 5 -.2667182 1 -.371666
      2 5 -.1285753 1 -1.

MPC 1000 5 2 -1. 1 2 1.371666
      1 4 .26671762 2 -.371666
      2 4 .12857513 2 -1.

MPC 1000 5 3 -1. 1 3 1.881468
      2 3 -.8814683 3 -1.

MPC 1000 5 4 -1. 1 4 1.371666
      2 4 -.3716663 4 -1.

MPC 1000 5 5 -1. 1 5 1.371666
      2 5 -.3716663 5 -1.

MPC 1000 5 6 -1. 3 6 -1.

MPC 1000 6 1 -1. 1 3 -.960235
      2 3 .9602349

SPC 1000 6 23456
    
```

```

$ DETECTOR
$ PRINCIPAL POINT
GRID 3 3 0. 0. 0. 3
$ DETECTOR COORDINATE SYSTEM
CORD2R 3 0 0. 0. 0. 0. 1.
      1. 0. 0.
$ INCIDENT OPTICAL AXIS COORDINATE SYSTEM
CORD2R 6 0 0. 0. 0. 0. 1.
      1. 0. 0.

$ ELEMENT 2
$ FIRST PRINCIPAL POINT
GRID 2 6 0. 0. .65972532
$ ELEMENT COORDINATE SYSTEM
CORD2R 2 6 0. 0. .65972530. 0. 1.659725
      1. 0. .6597253
$ INCIDENT OPTICAL AXIS COORDINATE SYSTEM
CORD2R 5 6 0. 0. .65972530. 0. 1.659725
      1. 0. .6597253

$ ELEMENT 1
$ FIRST PRINCIPAL POINT
GRID 1 5 0. 0. 3.2638961
$ ELEMENT COORDINATE SYSTEM
CORD2R 1 5 0. 0. 3.2638960. 0. 4.263896
      1. 0. 3.263896
$ INCIDENT OPTICAL AXIS COORDINATE SYSTEM
CORD2R 4 5 0. 0. 3.2638960. 0. 4.263896
      1. 0. 3.263896

$ OBJECT AT INFINITY AND NOT MODELED

$ MODEL PREPARED BY IVORY(TM) OPTOMECHANICAL MODELING TOOLS
$ Version 3.0
$ FOR Alson E. Hatheway Inc.
$ PROJECT NAME: 'TELE'
$ 11-20-2014 11:29:56
$ ALSON E. HATHEWAY INC., http://www.aehinc.com
    
```

MPCs use the influence coefficients to define the image motions.

93969_1.ppt, Unified Optomechanical Static Analysis, page 7

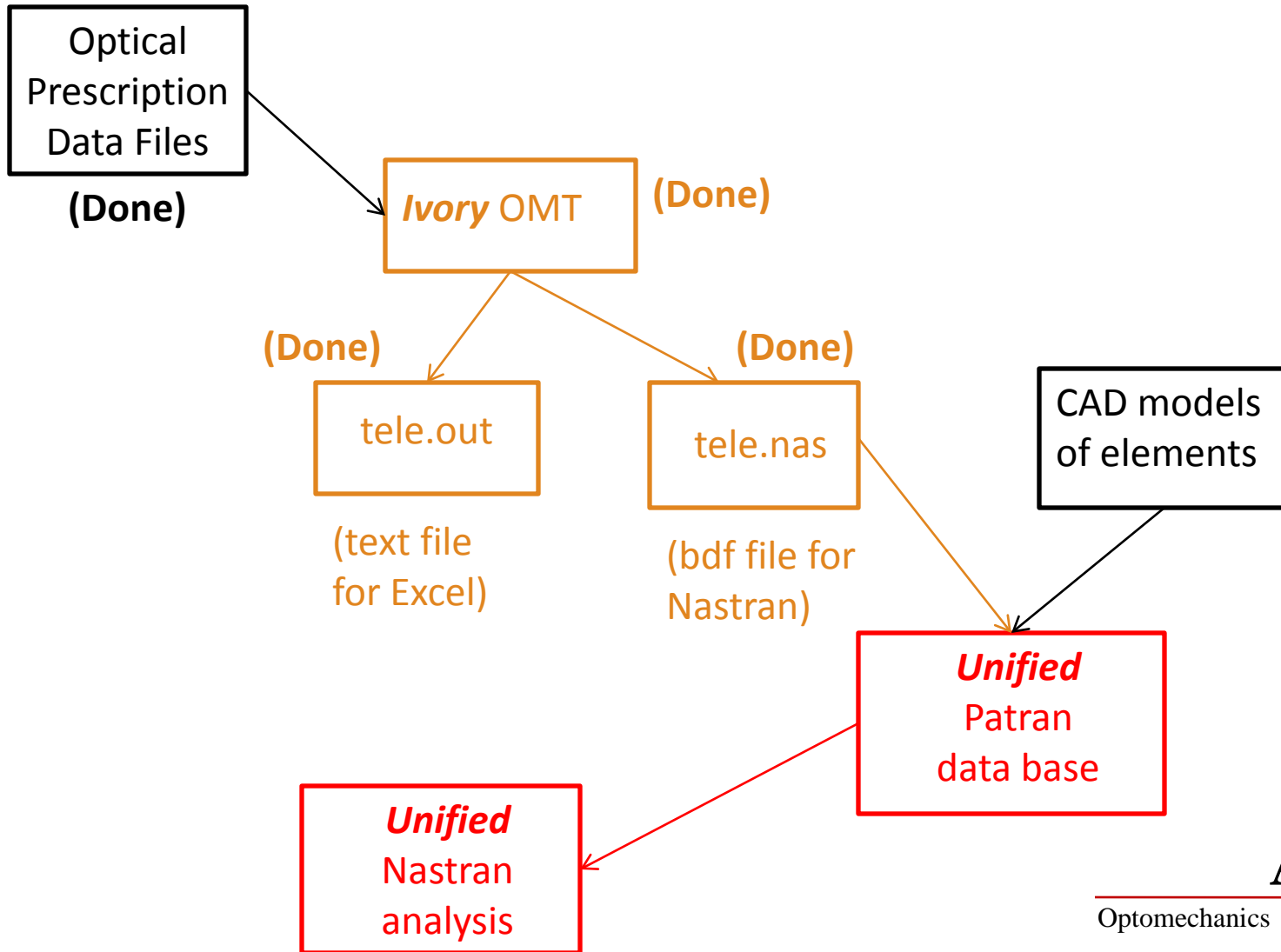
GRIDs and CORDs define the elements' positions and orientations.

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Optomechanics

They agree with the tele.out data file.

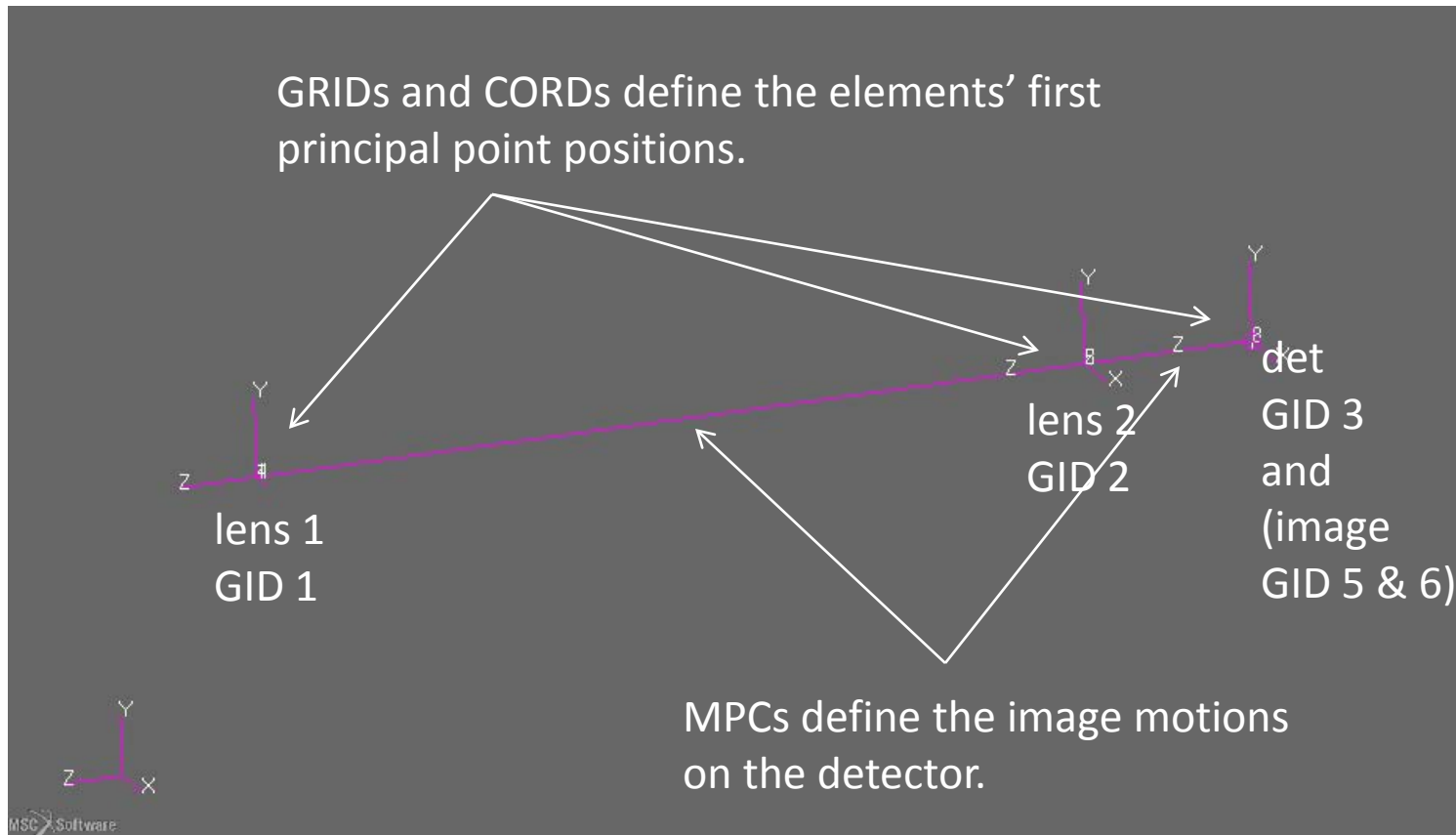
Generate the *Unified* Optomechanical Model



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Optomechanics

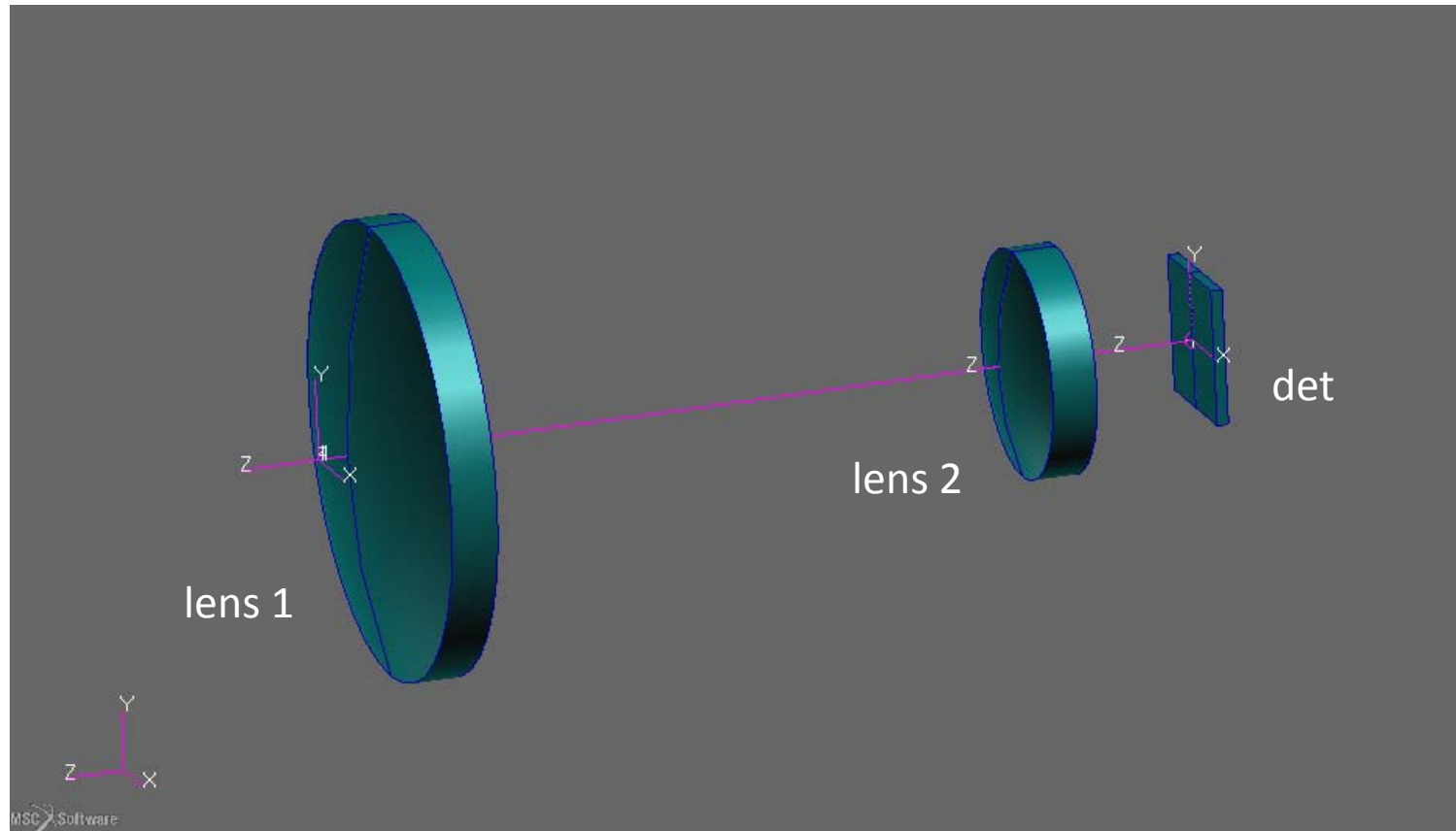
In Patran, Import the tele.nas File



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Optomechanics

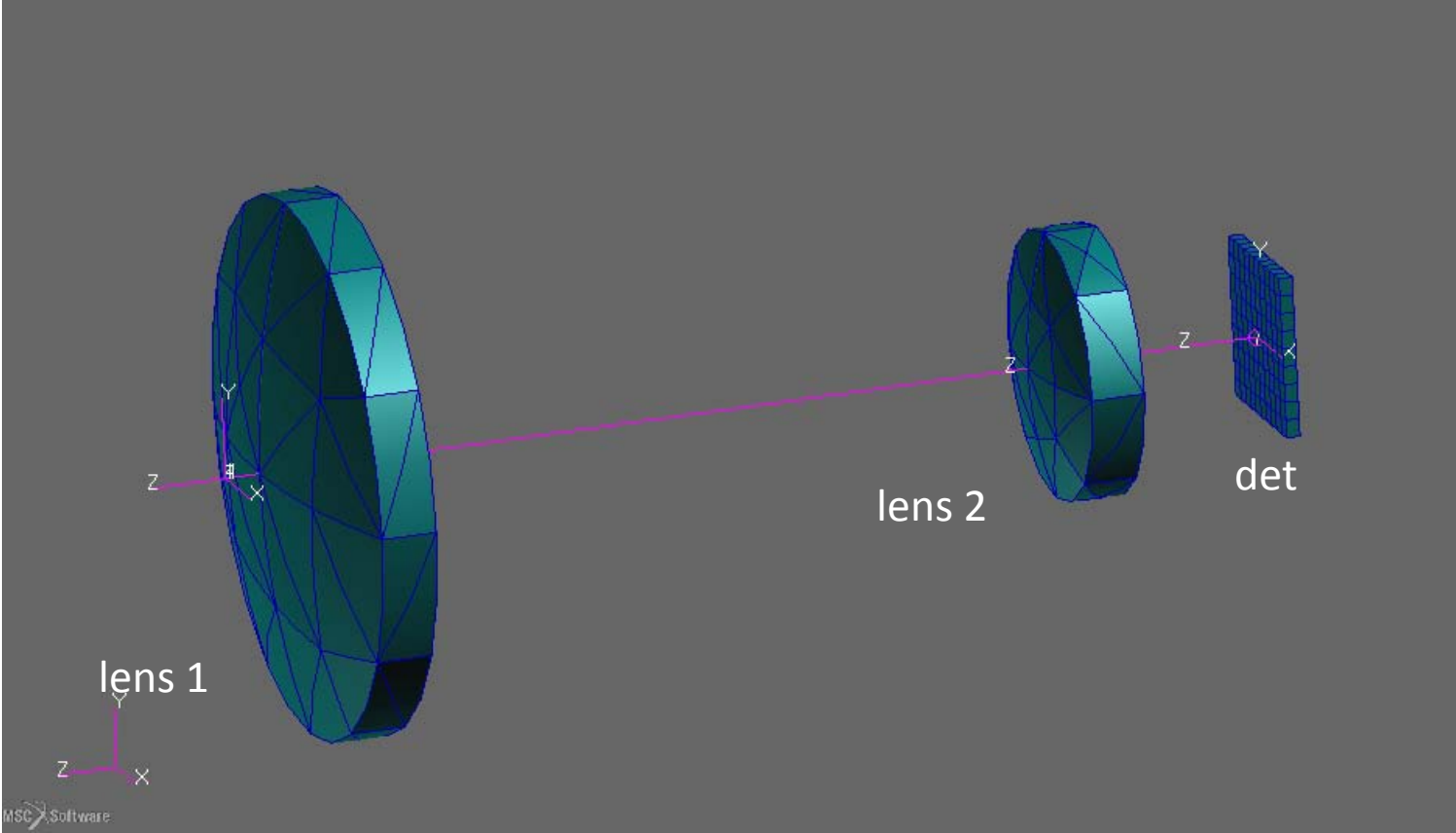
Then, Import the Lenses and Detector CAD Models into the **Patran** Model



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Optomechanics

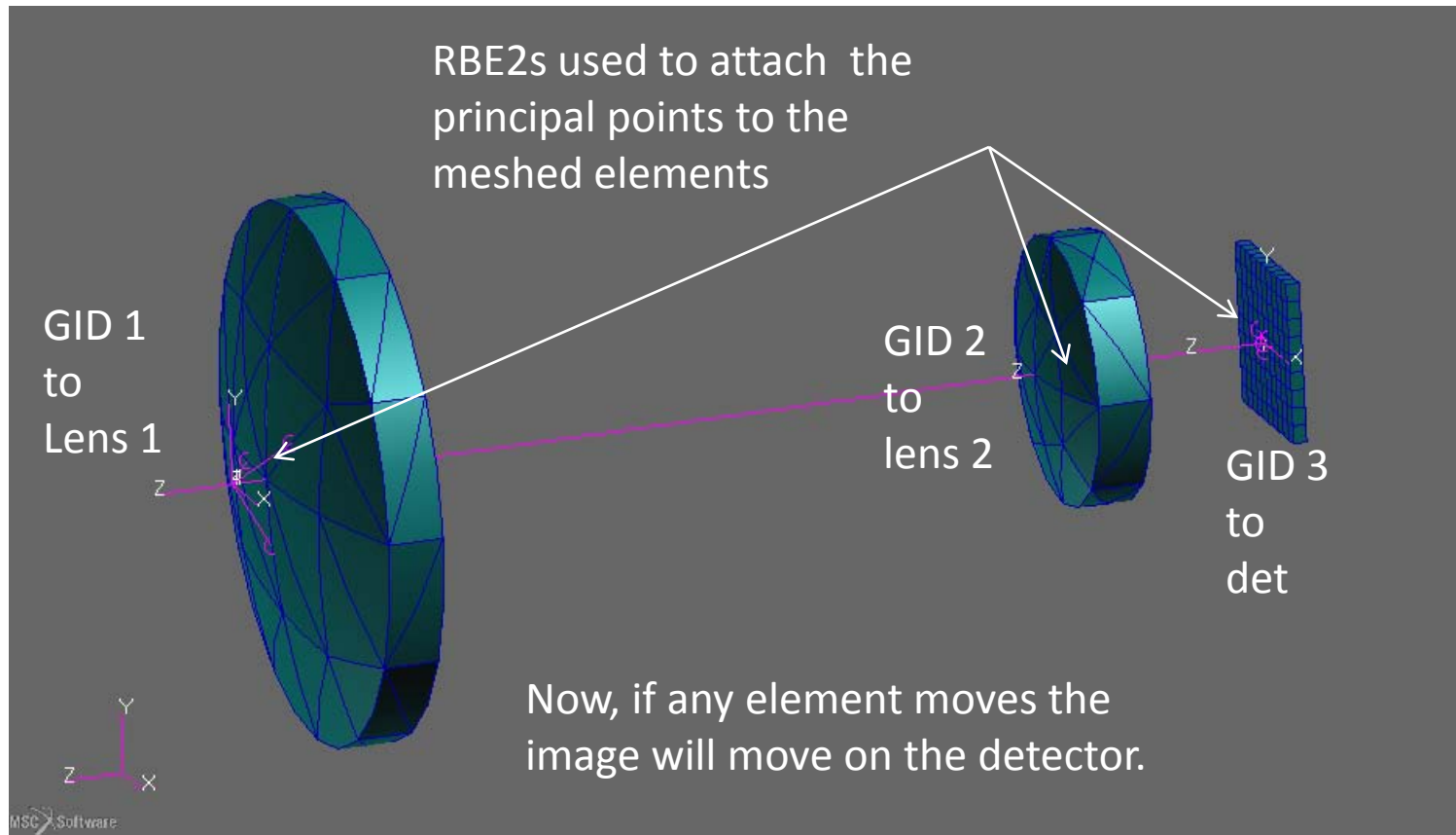
Mesh the CAD Models in Patran



AEH.

Optomechanics

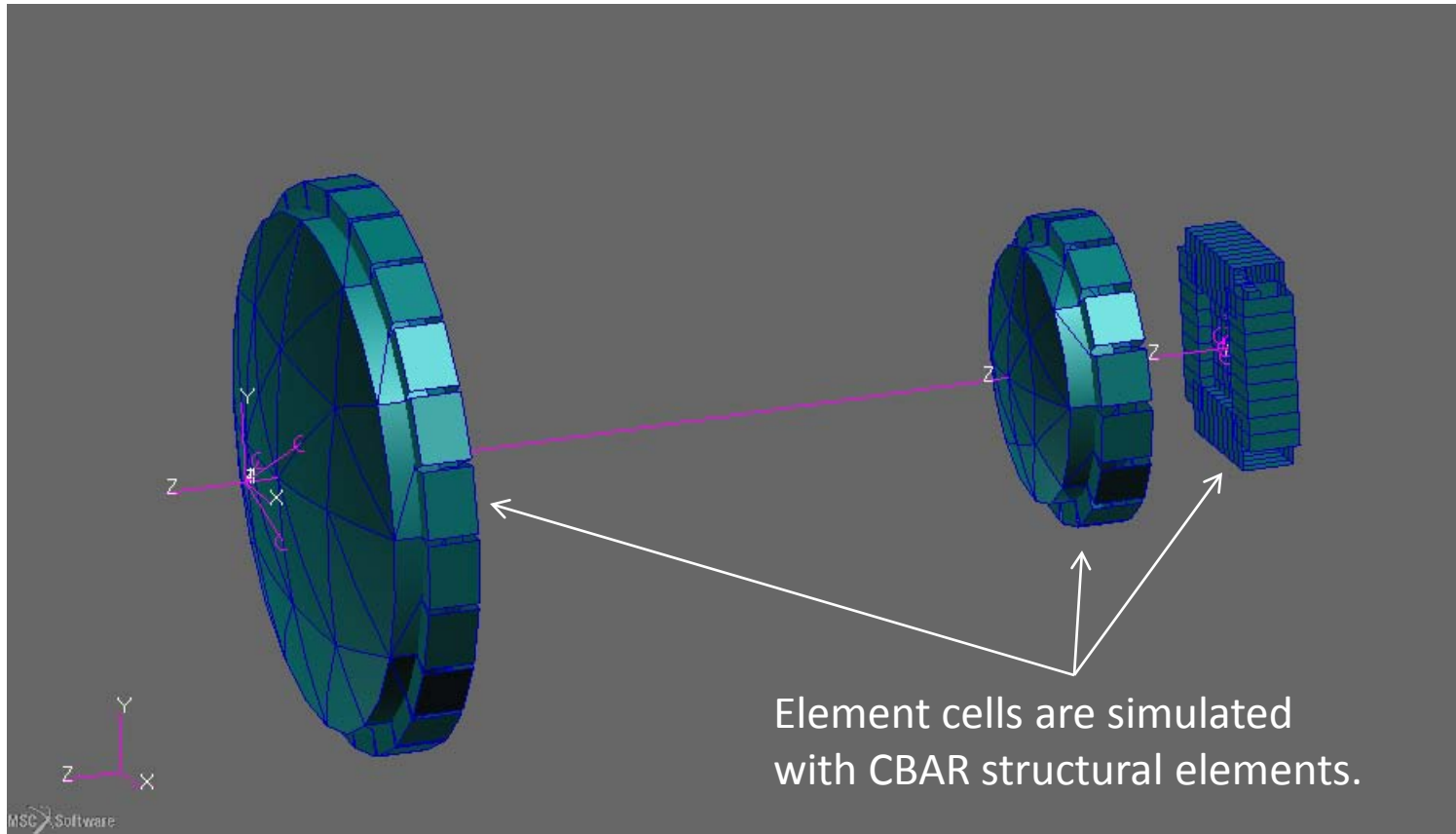
and Attach the Principal Points to the Meshed Elements in **Patran**



AEH.

Optomechanics

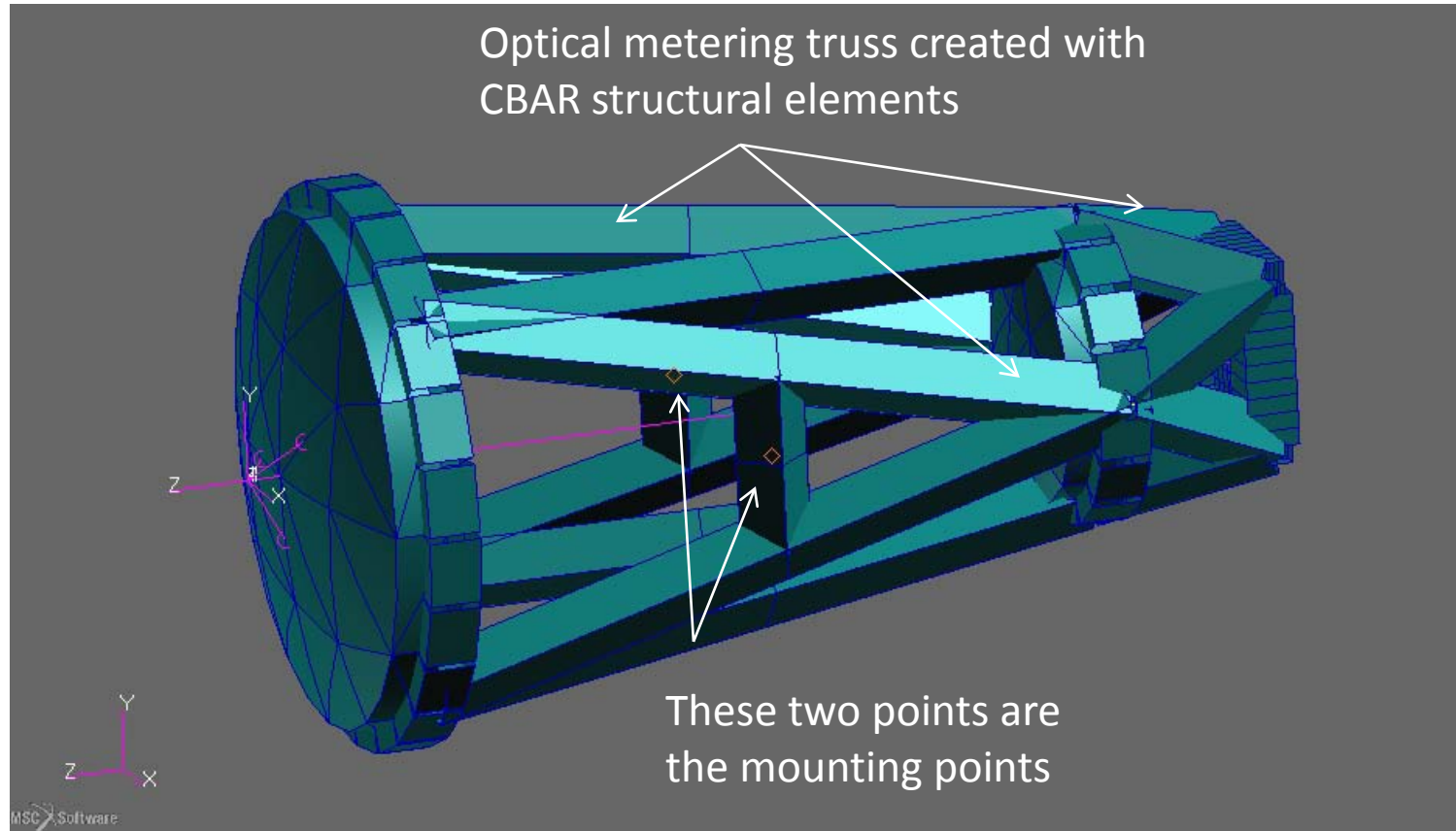
In **Patran** Create Cells for Each Element



AEH.

Optomechanics

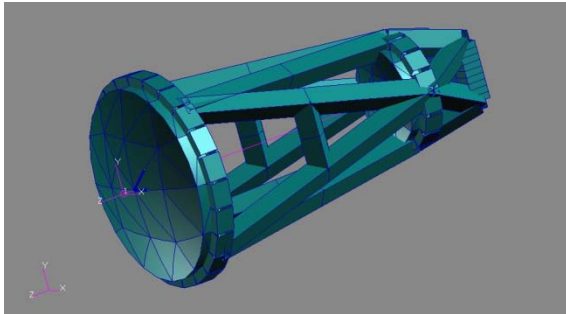
In **Patran** Create a Truss Structure for the Cells



AEH.

Optomechanics

In Nastran Run a 6 DOF Rigid Body Check



For unit displacements with an object at infinity the image motions should be either computational zeros, the focal length of the system (4.741172, see page 4) or -1.0 in the “tele.f06” file.

		D I S P L A C E M E N T V E C T O R						
POINT ID.	TYPE	T1	T2	T3	R1	R2	R3	
BASE MOTION:								
1.0 Tx	5 G	-1.239011E-10	9.571148E-12	-1.010361E-13	-1.980658E-13	-3.283262E-13	-9.969587E-12	
	6 G	3.545340E-14	0.0	0.0	0.0	0.0	0.0	
1.0 Ty	5 G	4.249783E-11	-8.842371E-12	5.046801E-13	4.182508E-13	4.095761E-13	-5.423809E-12	
	6 G	-2.176852E-13	0.0	0.0	0.0	0.0	0.0	
1.0 Tz	5 G	4.585644E-11	1.080863E-11	-1.085557E-12	-2.709695E-13	-6.882338E-13	8.544233E-13	
	6 G	4.827250E-13	0.0	0.0	0.0	0.0	0.0	
1.0 Rx	5 G	-8.676349E-11	-4.739557E+00	1.405411E-12	3.416156E-13	-1.469747E-12	1.259602E-11	
	6 G	7.719834E-13	0.0	0.0	0.0	0.0	0.0	
1.0 Ry	5 G	4.739557E+00	3.172970E-11	-9.775003E-13	-1.338907E-13	-3.279599E-13	1.546279E-12	
	6 G	4.457545E-13	0.0	0.0	0.0	0.0	0.0	
1.0 Rz	5 G	2.361326E-12	2.262890E-11	-3.414756E-13	-3.825188E-13	-9.552226E-14	-1.000000E+00	
	6 G	1.344123E-13	0.0	0.0	0.0	0.0	0.0	
REGISTRATION VARIABLES		TX	TY	TZ	RX	RY	RZ	
		DM/M						

GIDs 5 and 6 show the image motions.

AEH.

Optomechanics

In Nastran Analyze Optical Image Motions Due to X, Y and Z Axis Static Gravity Vectors in Nastran

1 DOUB'S IVORY(TM) UNIFIED OPTOMECHANICAL MODEL NOVEMBER 20, 2014 MSC.NASTRAN 1/26/09 PAGE 10
 0 X GRAVITY SUBCASE 1

DISPLACEMENT VECTOR

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	1.608140E-05	-4.240751E-08	-4.555795E-08	2.931421E-07	2.206466E-06	9.189821E-10
2	G	7.448824E-06	7.022216E-10	2.065525E-08	-1.122153E-07	1.105190E-06	2.692745E-08
3	G	6.956108E-06	8.417413E-10	-1.196107E-08	4.716450E-07	1.627794E-06	-2.378198E-08
5	G	1.160343E-05	4.476981E-09	-9.196381E-08	-2.783151E-08	9.880168E-07	2.378198E-08
6	G	6.357791E-08	0.0	0.0	0.0	0.0	0.0

1 DOUB'S IVORY(TM) UNIFIED OPTOMECHANICAL MODEL NOVEMBER 20, 2014 MSC.NASTRAN 1/26/09 PAGE 11
 0 Y GRAVITY SUBCASE 2

DISPLACEMENT VECTOR

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	-4.065706E-09	2.677417E-05	1.061671E-08	-9.334290E-06	-1.283125E-08	-1.461772E-08
2	G	3.189777E-09	-3.738374E-06	6.650016E-10	-8.295156E-06	2.750977E-08	1.446298E-08
3	G	1.190348E-09	-9.189099E-06	-1.882948E-09	-8.415510E-06	4.071022E-09	-2.324561E-08
5	G	-8.068579E-09	4.374857E-05	2.127209E-08	-1.305026E-06	-3.189704E-08	2.324561E-08
6	G	-9.555630E-09	0.0	0.0	0.0	0.0	0.0

1 DOUB'S IVORY(TM) UNIFIED OPTOMECHANICAL MODEL NOVEMBER 20, 2014 MSC.NASTRAN 1/26/09 PAGE 12
 0 Z GRAVITY SUBCASE 3

DISPLACEMENT VECTOR

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	-1.975805E-08	3.548287E-08	1.006376E-06	-1.880925E-07	-5.978592E-09	-7.007633E-08
2	G	-6.183997E-09	-5.286045E-10	8.377465E-07	-2.167514E-07	5.622505E-08	-1.054539E-08
3	G	-3.091442E-09	-1.129015E-09	8.114725E-07	-7.394736E-08	-4.540797E-09	3.566945E-09
5	G	-2.734813E-08	2.804116E-08	3.435514E-07	-1.034927E-07	-2.455889E-08	-3.566945E-09
6	G	-1.619185E-07	0.0	0.0	0.0	0.0	0.0

Optical element motions in black

Optical image motions in red

Image size changes

Displacement vectors from "tele.f06" Nastran output file.

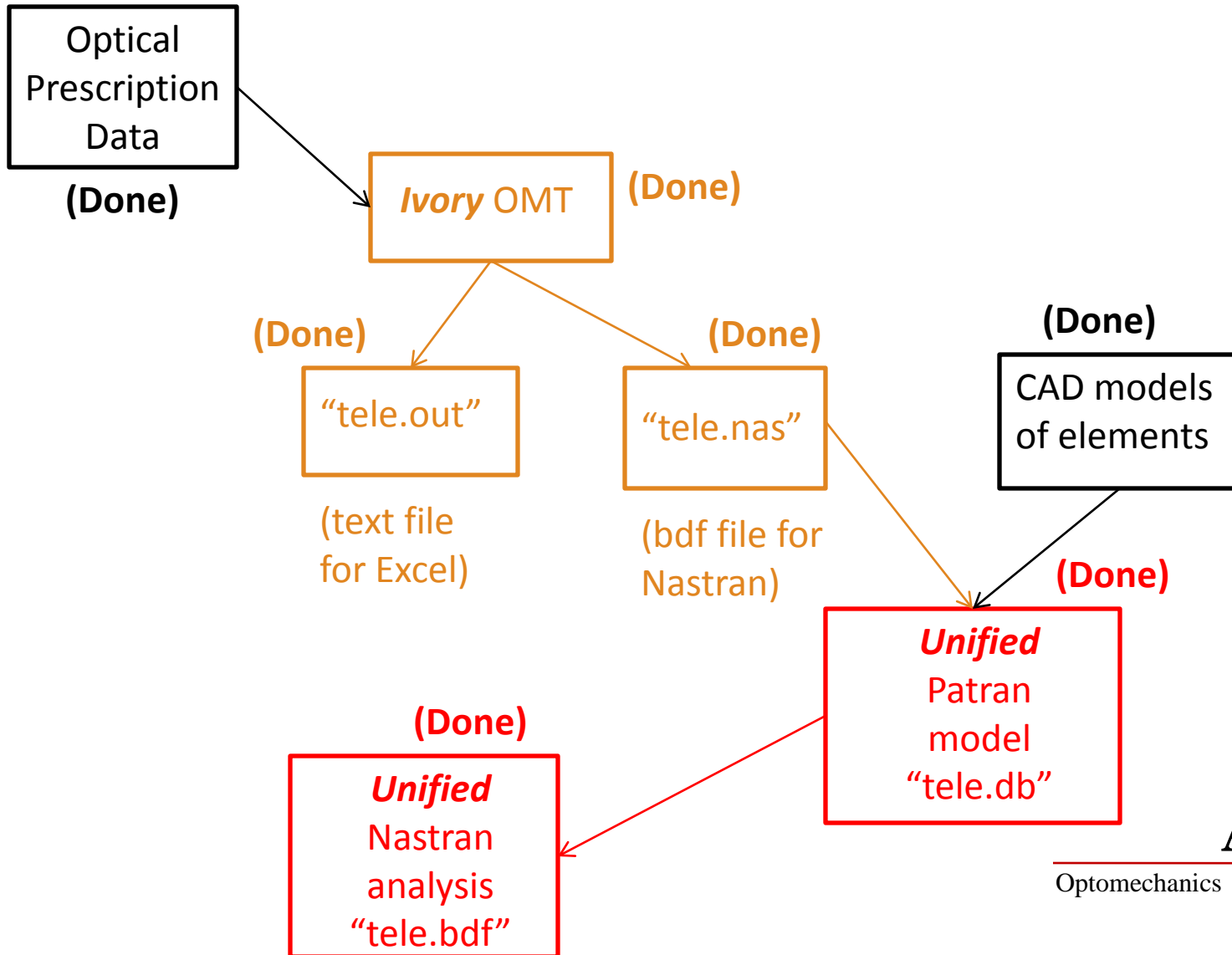
Stability of the (On-Axis) Image for 3 Axis Static Gravity

	Image lateral motion (X-Y Plane) micro-inches	Image focus motion (Z Axis) micro-inches	Image Size change ($\Delta M/M$)
X Gravity	11.6	-0.092	6.4 E-8
Y Gravity	43.7	0.0213	-9.6 E-9
Z Gravity	0.0392	0.344	-1.6 E-7

From “tele.f06” Nastran output file.
(Only translation effects reported here.)

AEH.
Optomechanics

Analysis with the *Unified* Optomechanical Model



AEH.

Optomechanics

Unified Optomechanical Static Analysis

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Prepare an *Ivory* optomechanical model from a telescope's optical prescription

Evaluate the optical faithfulness of the model in *Ivory's* output file

Import the *Ivory* optomechanical model into **Patran**

Import the CAD models of the optical elements into **Patran**

Attach the optomechanical model to the meshed optical elements in **Patran**

Construct lens cells in **Patran**

Construct a structural truss in **Patran** to support the lens cells

Check out the full model's optical quality with 6 DOF rigid body checks in Nastran

Analyze in **Nastran** the static gravity stability of the image on the detector

AEH.

Optomechanics